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PACKET RADIO COMMUNICATIONS. VOLUME 2

F. H. Dickson

Collins Radio Company

Prepared for:

Advanced Research Projects Agency

17 April 1974

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ABSTRACT			
Four major areas of activities in support of r			

Four major areas of activities in support of packet radio communications are reported in this document. These are: 1) evaluation and selection of radio link parameters for experimental packet radio system, 2) evaluation and selection of modulation and synchronization methods for experimental system, 3) equipment components analysis, 4) propagation/noise measurement equipment design data. Radio link parameter selection includes frequency range, data rates, antenna type, and expected ranges. Modulation and synchronization evaluation is based on both performance and implementation. Component evaluation consists of technological assessment in surface acoustic wave devices, RF sources, antennas, and microprocessors for packet radio application. A brief technical description and detailed design package including schematics and photographs of the propagation/noise measurement equipment are also reported.

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Propagation/Noise Measurement Equipment

4.1 INTRODUCTION

The purpose of this document is to provide a summary of the test objectives and characteristics of the ARPA packet radio propagation and noise measurement equipment. The main body of the volume is an overview and technical design summary. The details of the design are contained in the appendices.

The propagation test set has been designed to support the packet radio propagation measurement program. Emphasis in this test program is to be given to propagation characteristics that are most significant to transmission of digital signals. Measured data exists to predict path attenuation in the various environments in which the packet radio system is to operate, but there exists very little information relative to the multipath spread characteristics and the short period distribution of impulsive noise. These characteristics will have a significant impact on both system and equipment design for the packet radio systems. The propagation test set has been designed primarily to provide more information on these two important characteristics, and also provide facilities to measure net path loss and doppler spread. Since both the obstruction attenuation and noise level is expected to vary with frequency, measurements are to be made at two frequencies (430 and 1370 MHz).

The test set consists of a transmitter and receiver. The transmitter generates data bits at approximately 79 kb/s or 158 kb/s, which are then eode spread to a 10 M-chip or 20 M-chip modulation rate using a 127 chip maximal length code. The chips biphase modulate the two rf carrier frequencies. The 430 MHz output power is 10 watts and 1370 MHz, 6 watts. A high-gain omni antenna provides 2-dBi gain for 430 MHz and 9 dBi for 1370 MHz. Both frequencies can be radiated simultaneously.

The receiver has two fixed-frequency front ends but a common if. allowing only one frequency to be received at any one time. Surface Acoustic Wave Devices (SAWD's) provide demodulation and decoding for each data rate. The output data signal is correlation pulses of approximately 2 chips duration. For measuring doppler effects, all frequencies in the transmitter and receiver are phase locked to their respective precision frequency standards. The frequency standard in the receiver can be adjusted to obtain synchronization with the transmitter standard, thus allowing doppler frequency shift to be detected. For noise pulse measurements, a 50-dB dynamic range threshold detector is provided that operates at the if. frequency. One-tenth microsecond impulses can be detected and their level measured. The receiver antenna provides 2-dBi gain at both 430 MHz and 1370 MHz.

The time to design and build a test set was to be held to a minimum so that the collection of data could be started at the earliest possible date. A cost conscious, one-of-a-kind test set was constructed. Standard, available module packages were used to house the receiver and transmitter circuits. This was selected for design simplicity, flexibility, and minimum cost. The circuits contained in these modules are a mixture of printed circuit cards and board assemblies that have the components mounted on standoffs. The boards are non-standard Collins construction, but were selected as the most effective way to get the job done within the cost and schedule objectives. The flexibility of the equipment design and

construction has been of value in the test program, allowing modifications to satisfy test program requirements.

Problems arose during the building of the equipment with vendor parts availability and changes in the desired test set performance. The following is an overview of some of the performance problems and the corrective action taken:

The test set was originally designed and delivered to Stanford Research Institute to operate at 430 MHz and 1325 MHz. The 1325-MHz frequency under code spread occupies a 40-MHz bandwidth. Within that bandwidth are FAA flight control radars with high-gain directional antennas. The test set and the radars could not coexist. As an interim solution, a transmitter burst mode control was designed and built so that the test set transmitter could be synchronized with the radar sweep. The test set transmitter was inhibited when the radar was looking in its direction. This worked satisfactorily but the test set was later modified to operate at 1370 MHz.

Coexistence with other transmitters was also found to be a problem in the test set receiver at 430 MHz. In a per hertz bandwidth, some narrow band interfering signals appear at the receiver if. as high as 60 dB greater than the spread spectrum signal. The receiver was originally set to provide a desired signal at 0 dBm output from the 140-MHz if. The amplifier limits at +5 dBm, so even in the manual gain mode, the desired signal available to the SAWD's was much lower than planned (in the presence of interference) due to the limiting action and suppression of the weaker spread spectrum test signal. The receiver was modified to provide 13 dB more gain after the SAWD's so that the if. prior to the SAWD could be operated at lower gain and hence in a more linear region. Although there was an improvement, the dynamic range of the if. is still not adequate to coexistence at 430 MHz with some of the stronger narrow-band signals present in the test area.

A low side injection frequency (290 MHz) was used for the 430-MHz down-converter. A mixing product appears at 150 MHz within the dynamic range of the threshold detector which masks some of the noise data to be collected. The test set allows an external synthesizer signal to be injected into the down converter in place of the internal local oscillator. This was done to allow high-side injection and still retain phase lock with the 10-MHz receiver standard.

A phase jitter problem also became evident after the 1370-MHz conversion at SRI which affected doppler measurement. For the doppler tests, the external synthesizer approach was again used to provide an injection signal with low phase noise. This local oscillator phase noise problem will be corrected after testing by SRI is complete.

In summary, the test set was designed, fabricated, and modified on a short time schedule responsive to SRI's testing requirements. Although some problems were experienced with the test set, they were either corrected or the equipment flexibility allowed a fast effective alternative means of operation. The test set has not only provided the propagation and noise data for which it was designed, but also provided better insight into the problems of eoexistence between spread spectrum and conventional systems.

4.2 TECHNICAL DESCRIPTION

4.2.1 Elements of the Test Set

The following lists the major items of the test set, CPN 627, 9553-001

Items	Collins Part Number
Transmit Subsystem	
Transmitter CW Transmitter Control Burst Mode Control Antenna 9 dBi at 1370 MHz, 2 dBi 430 MHz 2 dBi at both frequencies Receive Subsystem	$\begin{array}{c} 627 - 9561 - 001 \\ 627 - 9562 - 001 \\ 631 - 7575 - 001 \\ 627 - 9502 - 001 \\ 627 - 8137 - 001 \end{array}$
Receiver Receiver Power Supply Antenna Threshold Detector	627-9541-001 627-9555-001 627-8137-001 627-9564-001
Miscellanous Cables	627-9563-001

The transmitter is packaged in a weather protective box for mounting on a pole. A bracket on the transmitter allows convenient antenna mounting. Cables were provided to allow installation of the controls inside a building.

The receiver subsystem is mounted with SRI equipment. The threshold detector module was integrated into one of their panels. The power supply and receiver are 19-inch panel mount units.

4.2.2 Transmitter Characteristics

Figure 4-1 shows the block diagram of the transmit system. Figures 4-2 through 4-4 show the transmitter, transmitter control, and the burst mode control, respectively. The control panel is essentially a grouping of switches that control power and termination of four TTL mode control lines. Remote control is also available by selection. The burst mode control contains a variable rate generator to determine cycle time and a duration timer to select the duty cycle of the transmitter. The rate generator can be operated from an external sync derived from a cyclic radar or other user with which the test set must coexist. The rate generator range is continuously variable from 0.25 to 20 Hz in the cycle mode. The burst durations are selected to be 20, 40, 80, 160, 1000, and 5000 μ s long. The burst control gates the TTL mode control lines from transmitter standby code to whatever mode was selected on the control panel. A light on the front panel indicates when the transmitter is enabled.

The transmitter contains a precision 10-MHz frequency standard and a 430-MHz and 1370-MHz oscillator phase locked to the standard. The rf frequencies are supplied to balanced mixers which biphase modulate the carrier according to the code generator chip data. Each biphase modulated output is amplified and radiated from its own set of dipole elements in a colinear antenna mast. The transmitter antenna gain is 2 dBi at 430 MHz and 9 dBi at 1370 MHz. The antenna is shown in figure 4-5.

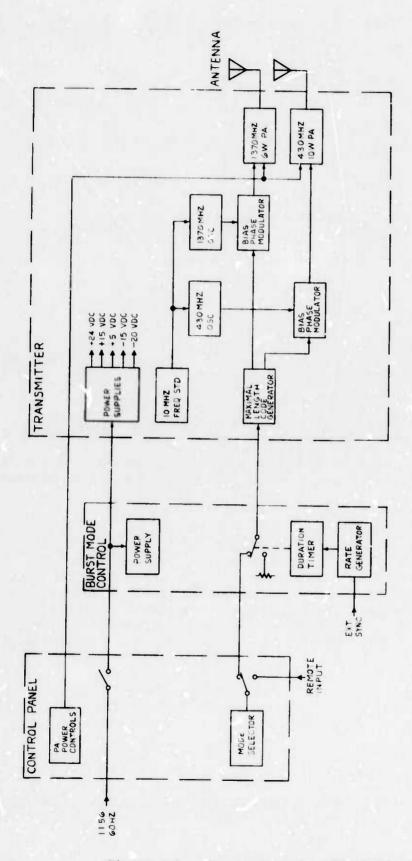


Figure 4-1. Transmit System Block Diagram.

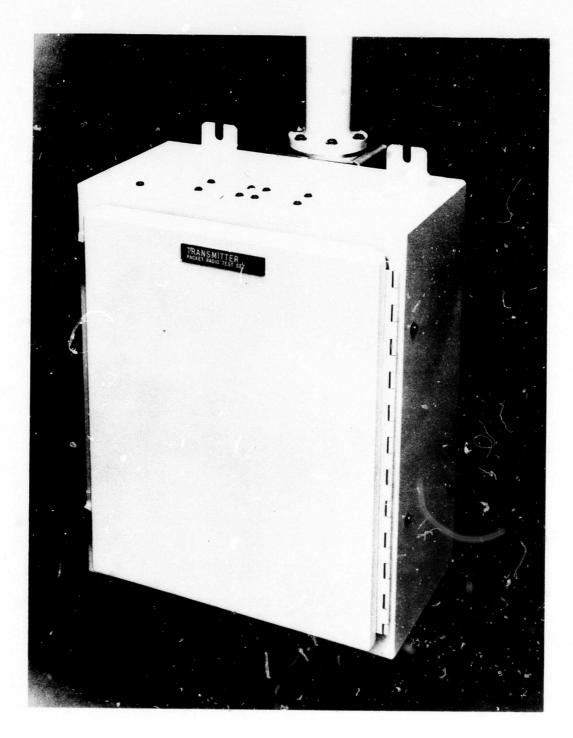


Figure 4-2. Transmitter.



Figure 4-3. Transmitter Control.

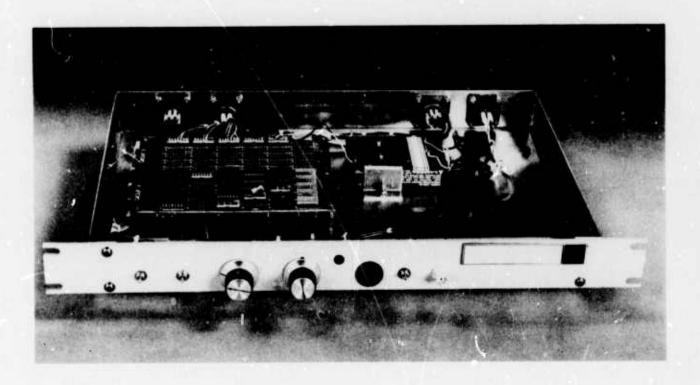


Figure 4-1. Burst Mode Control.

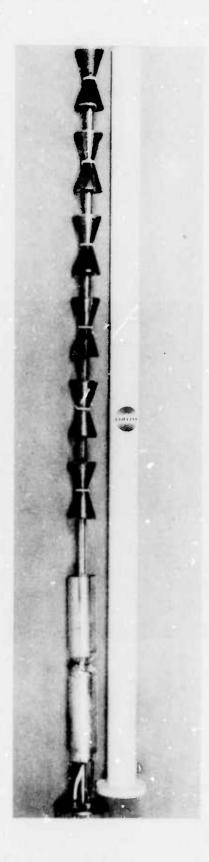


Figure 4-5. High-Gain Antenna.

4.2.3 Receiver Characteristics

Figure 4-6 shows the receive system block diagram. Figure 4-7 shows the front panel of the receiver which is arranged to aid an operator in understanding the signal flow without studying the schematics or detailed system diagrams. Maximum flexibility is provided at the receive front panel to monitor signals or inject signals. The 10-MHz frequency standard is available for reference input to an external synthesizer that can be used to generate injection frequencies for the down-converters. The if, is available to be used with a spectrum analyzer to monitor the received signal and interference. The receiver outputs are available at the rear of the unit and also available on the front panel.

The receive system antenna is a low-gain, colinear, dipole antenna with separate dipoles for 430 MHz and 1370 MHz. Each dipole yields a 2-dBi gain. The antenna construction is shown in figure 4-8.

Each receive frequency has its own rf front end consisting of a 3-pole, 50-MHz bandwidth filter and a low-noise rf amplifier. The down converters are double balanced mixers followed by 140-MHz if. preamplifiers. The receive channel select function chooses if. preamplifier output is selected for detection. When the selection is made, power to the rf amplifier and if. preamplifier of the unselected frequency is turned off.

The if. bandwidth can be either 50 MHz or 500 kHz. If the 500-kHz bandwidth is selected, gain is added in the if. switching module to compensate for reduced noise bandwidth. As a result, the noise threshold detectors operate at a fixed level of spectral density independent of the bandwidth setting.

The if, age amplifier maximum gain is > 60 dB and can be adjusted manually or by age for -13-dBm output. This gain plus the front end gain of approximately 30 dB allows thermal noise to be amplified to the -13-dBm level, thereby providing adequate gain for any usable signal.

The SAWD correlators provide approximately 20 dB of processing gain so that 0 dB input signal-to-noise levels will provide useful output. The if, frequency is actually 139,98 MHz due to the manufacturing tolerance of the SAWD's. The detector has a 13-dB linear dynamic range from the maximum output level of approximately 5.0 volts peak. The detector output impedance is 50 ohms.

The doppler test function compares a received CW signal converted to 140 MHz if, and a 140-MHz frequency obtained from a local oscillator phase locked to the precision 10-MHz frequency standard. The frequency standard can be manually synchronized with the transmitter frequency standard or locked through a very slow phase-lock loop for short period doppler measurements. The bandwidth for measuring doppler is approximately 100 Hz.

The down-converter injection frequencies are also phase locked to the precision $10\text{-}\mathrm{MHz}$ standard.

The threshold detector consists of six stages of amplification at 140 MHz. Each amplifier has a detector and comparator that will level detect noise impulses of less than 0.1 μs in duration. Each stage adds 10 dB of gain so that 0 to -50-dB levels in 10-dB steps are detected. Since the radio gain preceding this module is approximately 30 dB, noise impulses from -30 to -80 dBm can be monitored. The detector outputs are differential MECL integrated circuits. A secondary output allows the detected outputs to be monitored on the front of the receiver. This is of value for threshold level calibration.

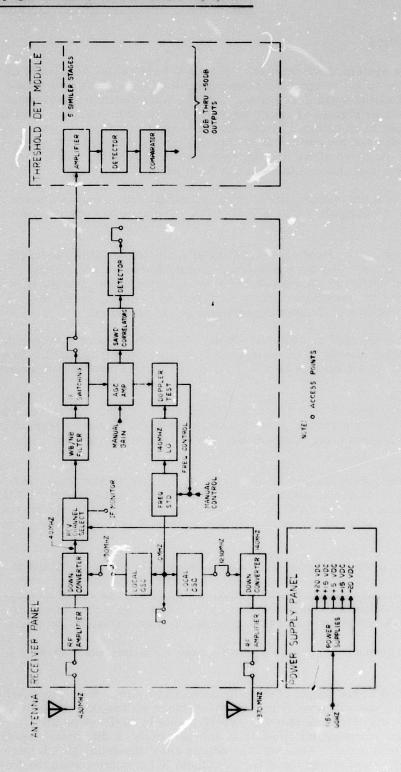


Figure 4-6. Receiver System Block Diagram.

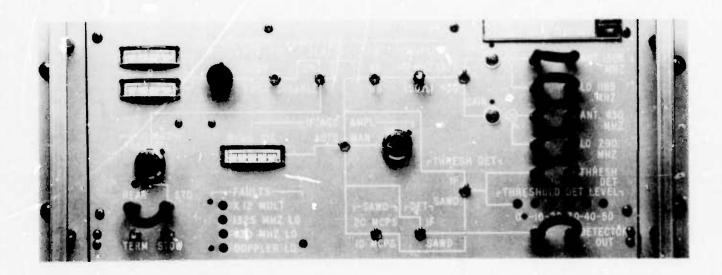


Figure 4-7. Receiver System Front Panel.

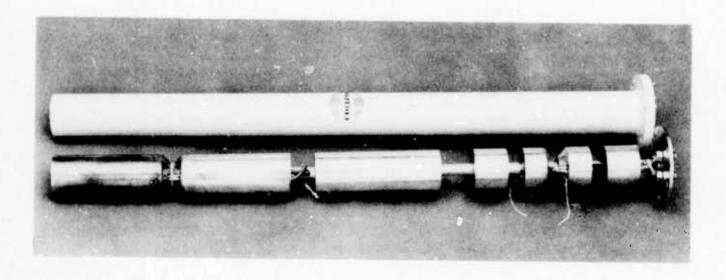


Figure 4-8. Low Gain Antenna Construction

4.2.4 Specification Summary

TRANSMITTER AND CONFROL

Frequency Bands -430 MHz and 1370 MHz

Output Power -430 MHz - 10 W

-1370 MHz - 6W

2 Pole 40 MHz BW centered on output frequencies Output Filters

Modulation Biphase at a 10 M-chip or 20 M-chip rate

Frequency Stability All frequencies locked to 10-MHz standard

<5 x 10^{-10} /day after 24 hour warmup Aging Rate

 1×10^{-11} for 10 seconds average time Stability

 $< 1 \times 10^{-9}$ over 0 to 70°C. Temp Coefficient

Within 5×10^{-9} of final frequency in 15 minutes Warmup

after turnon at 25°C

Data Rate 78.74 kb/s and 156.48 kb/s

Coding 127 chip maximal length code

Input Power 115V 60 Hz

Controls (Front Panel)

Power On-Off

430 MHZ PA On-Off

1370 MHZ PA On-Off

Mode Control

ABCD	CONTROL OPTIONS
TTL LEVEL CONTROL INPUT	RESPONSE
0000	STANDBY, CARRIER OFF
0001	140 MHZ CW (DOPPLER)
0010	CONTINUOUS PRN, 10 MHZ
0011	CONTINUOUS PRN, 20 MHZ
0100	CODE/1 BLANK, 10MHZ
0101	CODE/1 BLANK, 20 MHZ
0110	CODE/3 BLANK, 10 MHZ
0111	CODE/3 BLANK, 20 MHZ
1000	CODE/1 CARRIER, 10 MHZ
1001	CODE/1 CARRIER, 20 MHZ
1010	CODE/3 CARRIER, 10 MHZ
1011	CODE/3 CARRIER, 20 MHZ

Local Remote Mode Selection

propagation/noise measurement equipment

Indicators (Front Panel) Power On

Fault Summary

Note — The control panel fault is a loss of phase

lock of any of the phase-locked loops.
Individual loop indicators are inside the

transmitter cabinet

Antenna(s) High gain omni colinear must

1370 MHz 9 dBi 430 MHz 2 dBi

Optional antennas

A directional 10-dBi horn for 1370 MHz was pro-

vided to SRI

A 2 dBi low-gain antenna same as the receiver

antenna was also provided.

BURST CONTROL PANEL

Note that this panel is required only if the system is to be operated in the burst mode. The cables from the transmitter will connect directly to the control panel or can be fed through the burst mode control.

Power 115V 60 Hz

Repetition Rate 0.25 Hz to 20 Hz (continuously variable)

Burst Duration (s) 20, 40, 80, 160, 1000, and 5000 µs

Controls (Front Panel) Repetition rate

Burst duration

Mode (s)

Cycle or single burst

Normal or burst mode

Sync button which initiates single burst

Sync internal - external

Indicator (Front Panel) Rate light that shows when transmitter enabled.

RECEIVER

Receive Signal Range 0 to -90 dBm

Frequency Bands 430 MHz and 1370 MHz

RF Filters 3 pole 50 MHz BW centered on receive frequencies

RF Amplification > 12 dB (noise figure < 3.5 dB)

Receiver Noise Figure < 8 dB

IF. Frequency 139.980 MHz

IF. Gain >60 dB

Demodulation and Decoding 10 M-chip and 20 M-chip SAWD's; 127-chip maximal length code biphase modulation construction

Processing Gain 20 dB

Frequency Stability Same as transmitter

For doppler tests, the frequency standard can be

electrically shifted ≥ 1 x 10-7 ppm

Doppler Test Bandwidth 100 Hz

Input Power 115V 60 Hz

Outputs 10 MHz frequency standard 0 dBm 50Ω

IF output (Input signal level plus approximately

30-dB gain, 50Ω)

Detected signal out 5V peak from 50 Ω source

Analog agc level (0 to +15V)

Doppler I&Q outputs (each $0 \pm 5V$)

Controls (Front Panel)

Gain To balance rf receive level of 430 MHz and 1370 MHz

Bandwidth Selection 50 MHz or 500 kHz

AGC Amplifier Automatic (-13 dBm output) or manual.

Manual AGC Gain 10 turn pot for > 60-dB range

SAWD Selects output from 20 M-chip or 10 M-chip SAWD

Detector Selects whether the if. or SAWD output will be

detected

Threshold Detector IF-SAWD

Only the if. signal is now available for switching. The SAWD signal is available at the STOW SMA connector and can be patched to the threshold

detector.

propagation/noise measurement equipment

10-MHz Frequency

Control

Shifts 10-MHZ frequency standard

Doppler Test

In ON position causes doppler unit to control the 10 MHz frequency standard to obtair synchroniza-

tion with transmitter.

10-MHz Phase

This controls the phase lock angle after doppler

synchronization.

ØLL Time Constant

Controls setting time, of synchronization

Indicators (Front Panel)

Doppler I&Q channels

Receive Signal Strength - Only operational in auto

agc mode

Faults - Loss of phase lock for the receiver loops

Threshold Detector - Sense monitors

Threshold Detector

0 to -50-dBm range in 10-dB steps

Output - Differential MECL levels for each 10-dB

level detector

Response time < 20 ns

Antenna

Colinear 430-MHz and 1370-MHz dipoles each

2-dBi gain

Design Details

A. 1 INTRODUCTION

This appendix contains pictures of the test set and detailed schematics of the equipment. The pictures reflect a variety of construction techniques from printed circuit cards to brass board type modules. This construction is not Collins normal practice, but was the most cost-conscious and efficient means to provide a usable one-of-a-kind test set in a minimum amount of time. The schematics represent the circuits as they exist as of this report. The pictures and schematics are felt to be self-explanatory and are thus presented without narrative in the order shown in the index for this appendix.

NOTE

In some cases, 1325 MHz and 1370 MHz are both shown in the documentation. Due to coexistence problems at 1325 MHz, the test set frequency was changed to 1370 MHz. Any reference to 1325 MHz should be interpreted as being the 1370-MHz channel.

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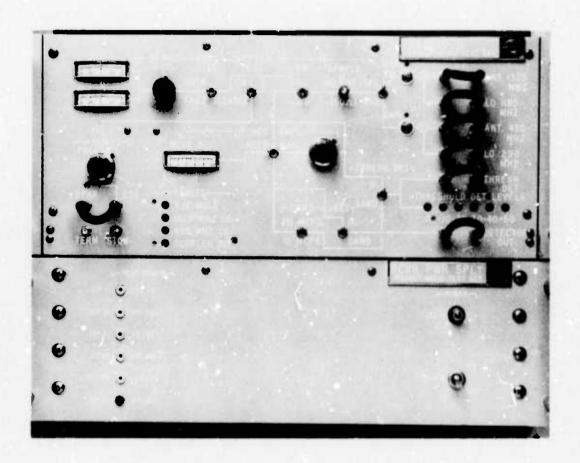
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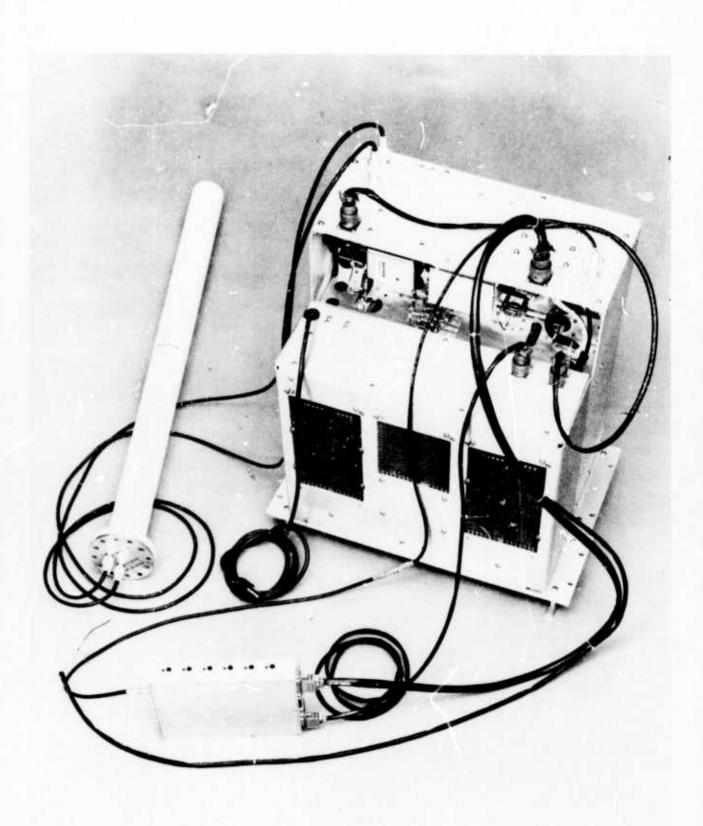
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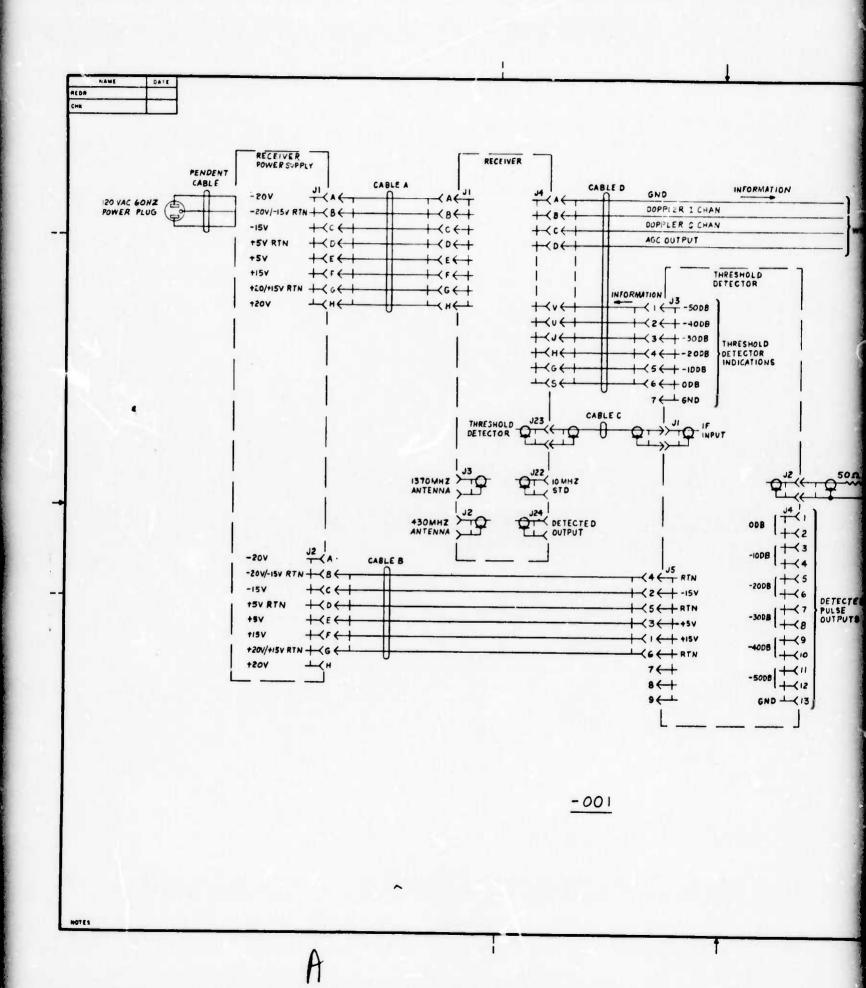
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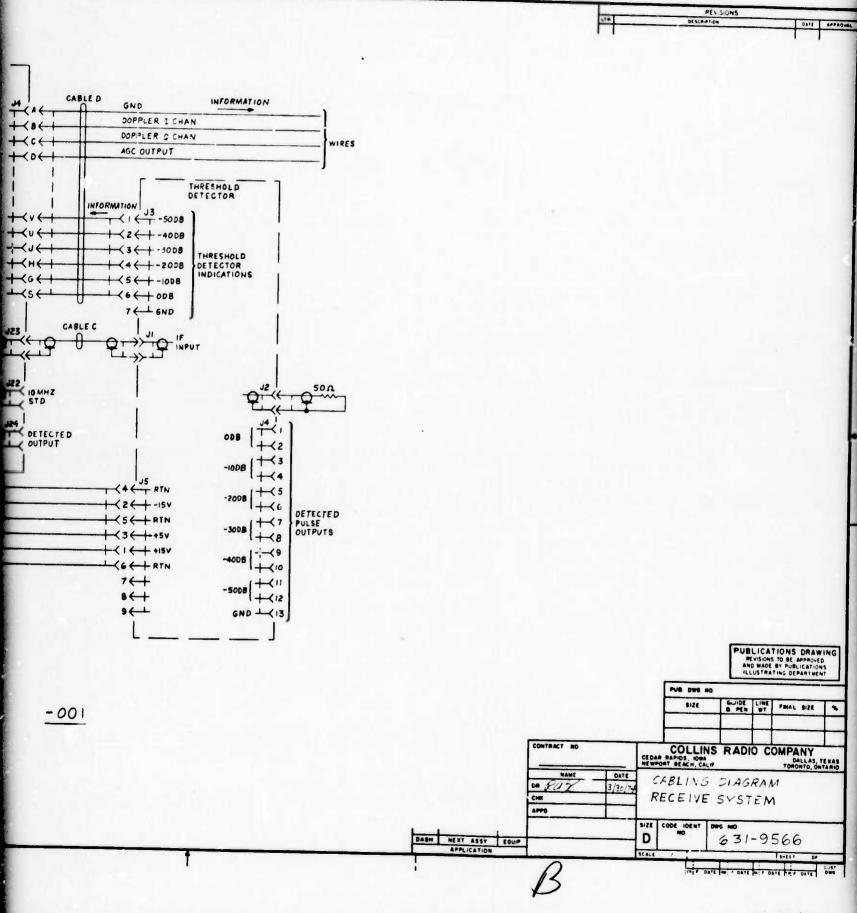


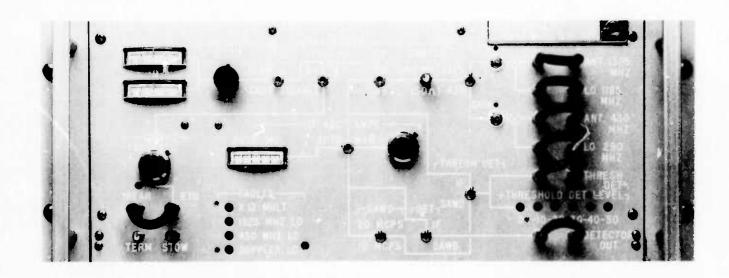
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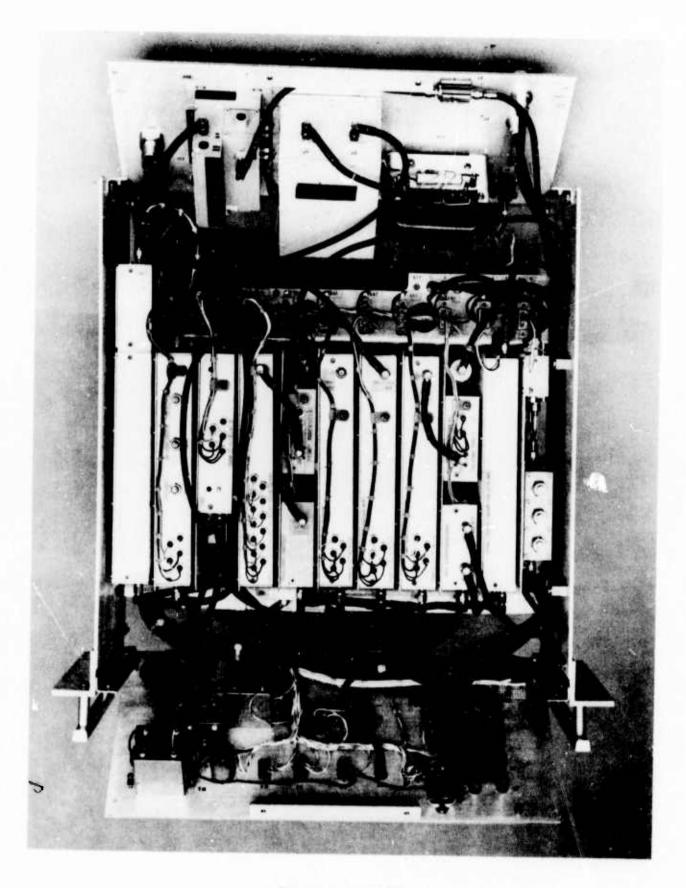
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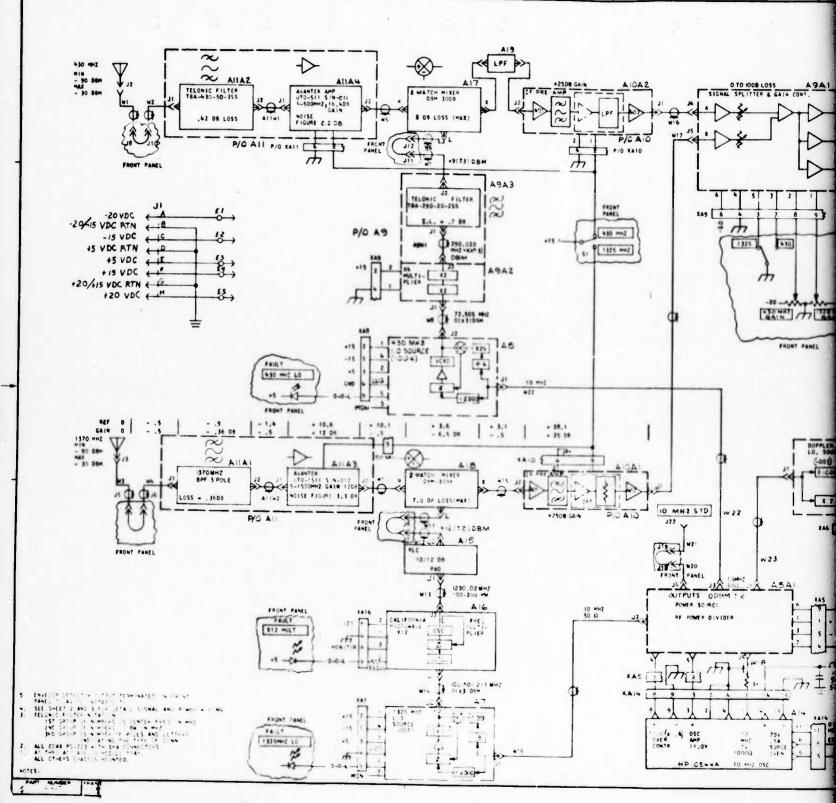




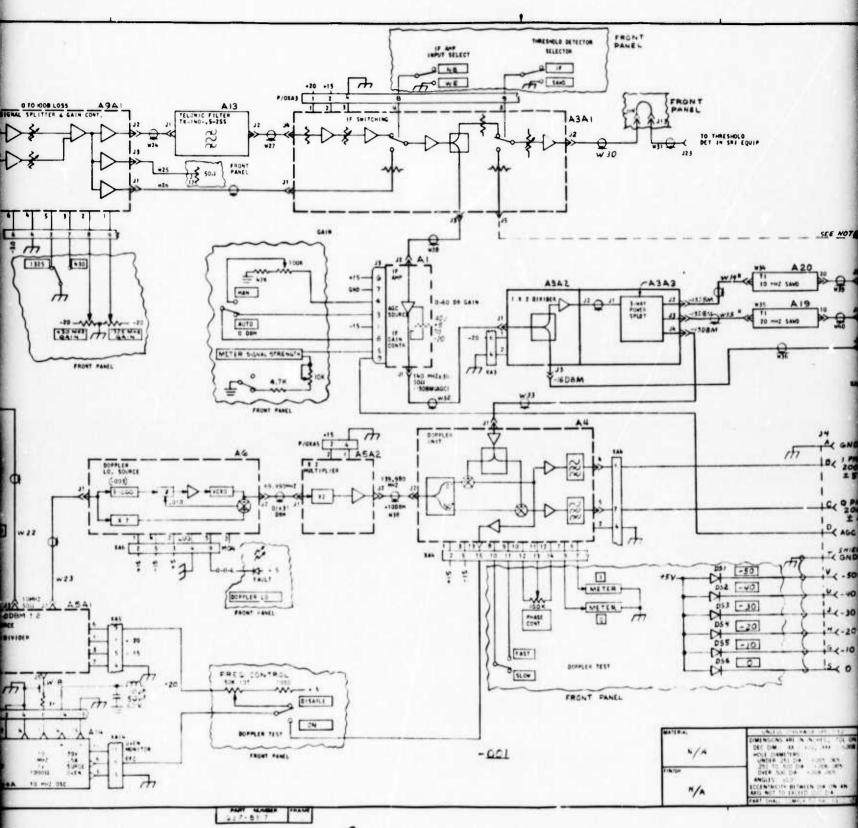
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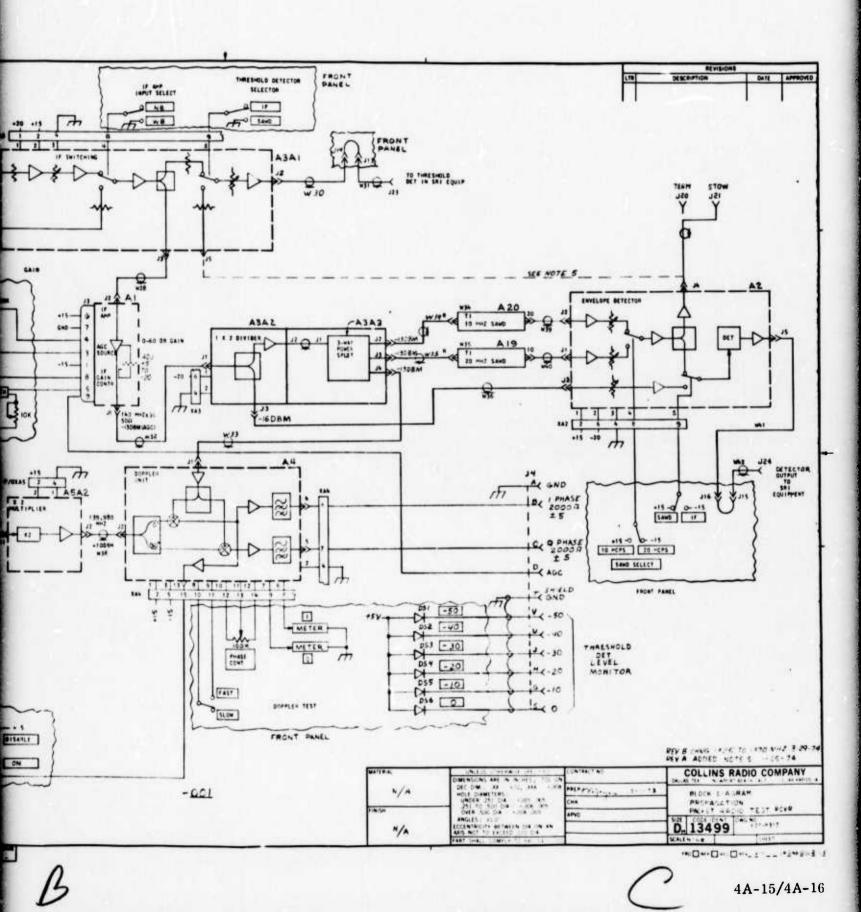
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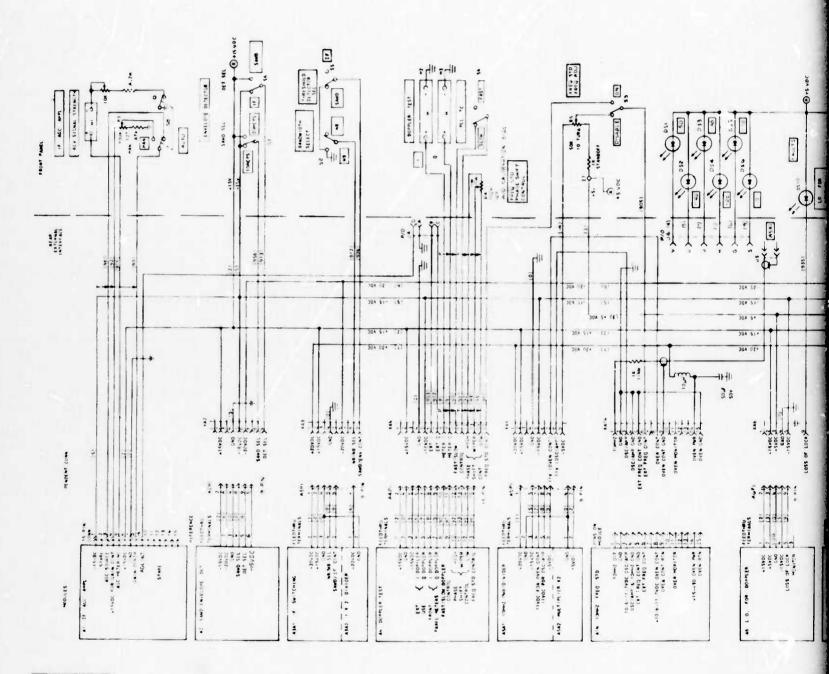


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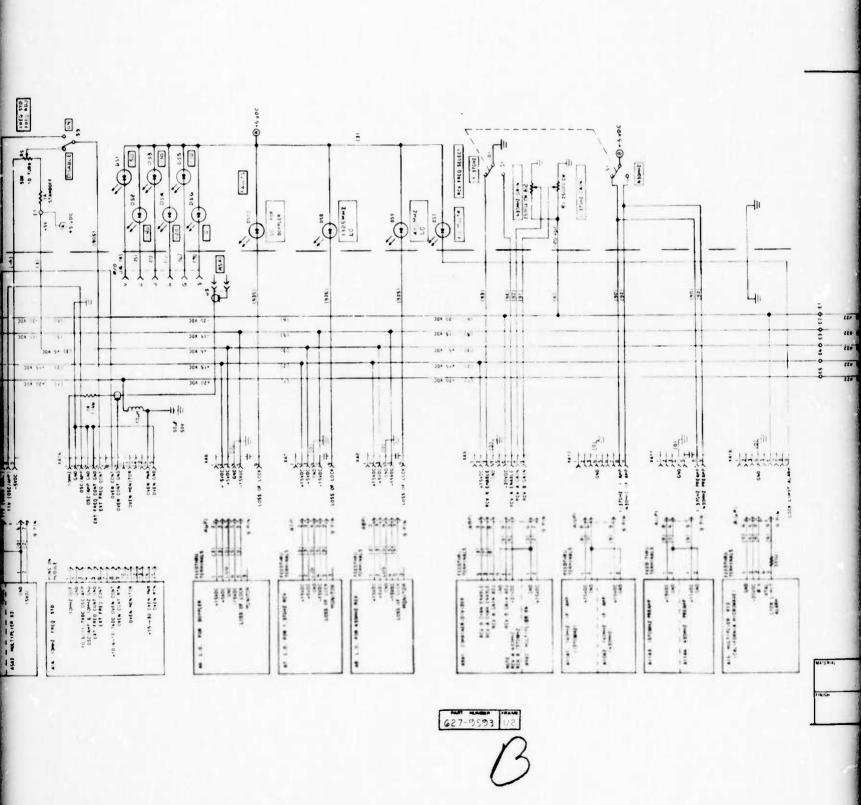
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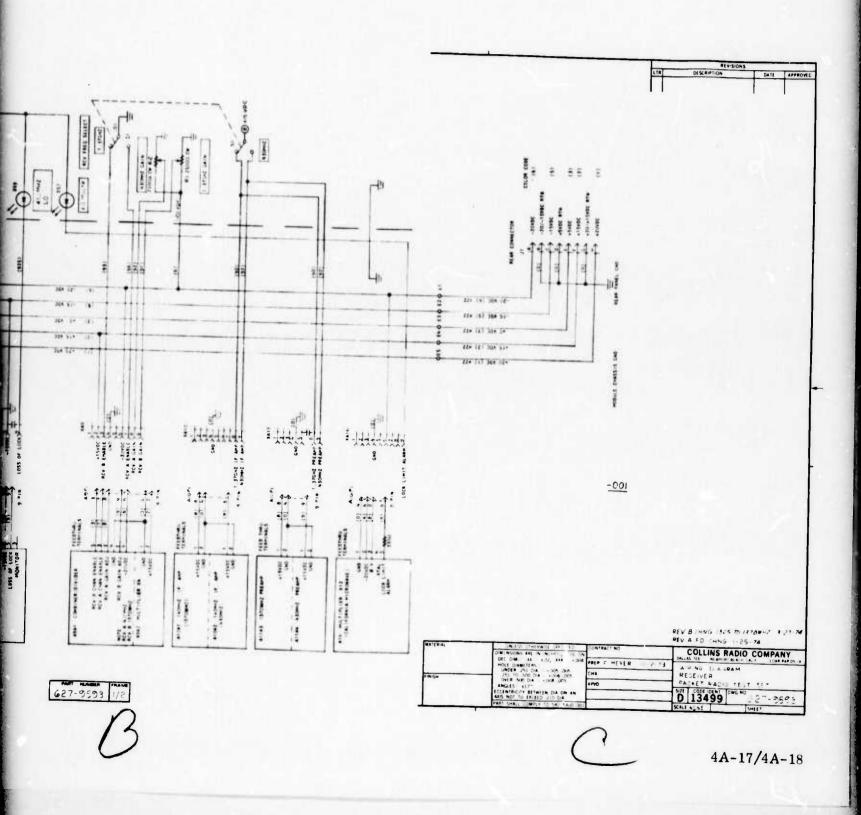


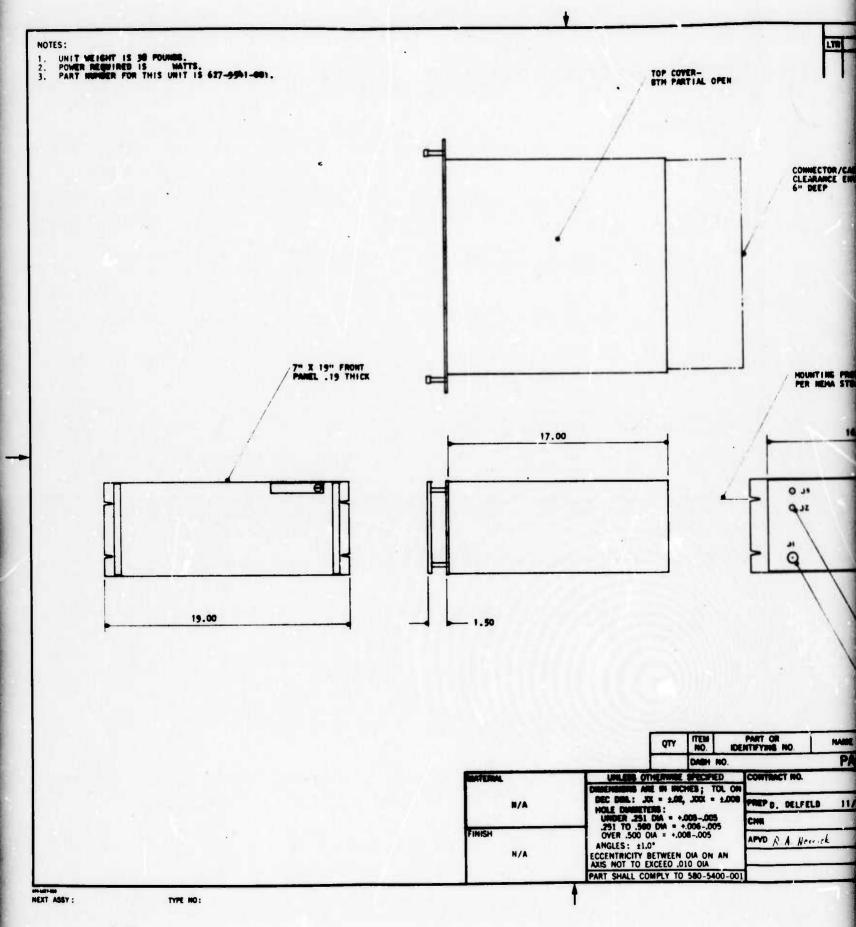


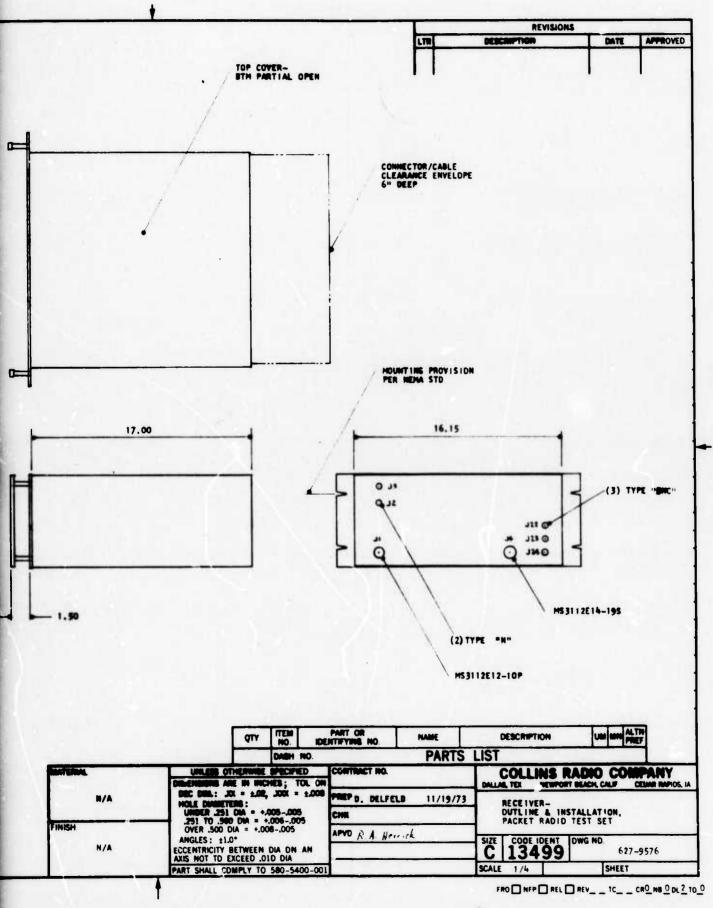
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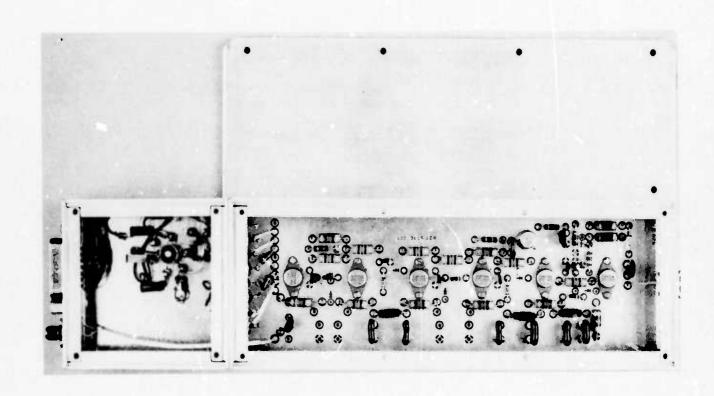


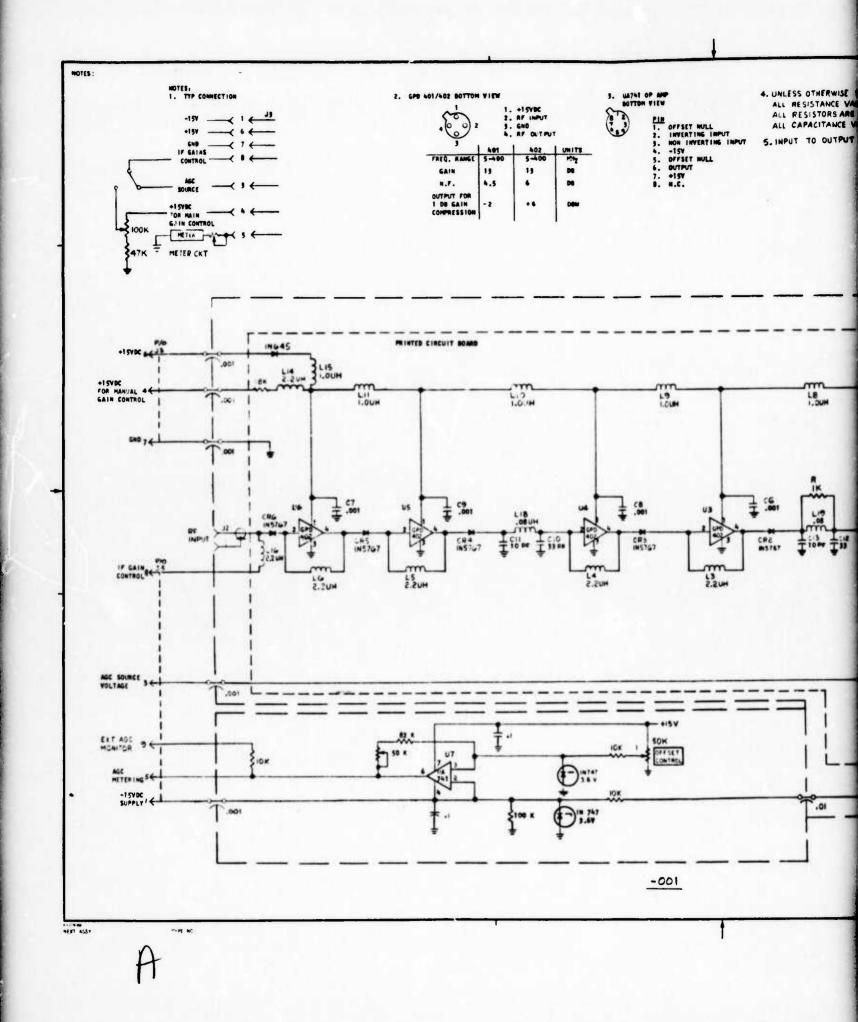


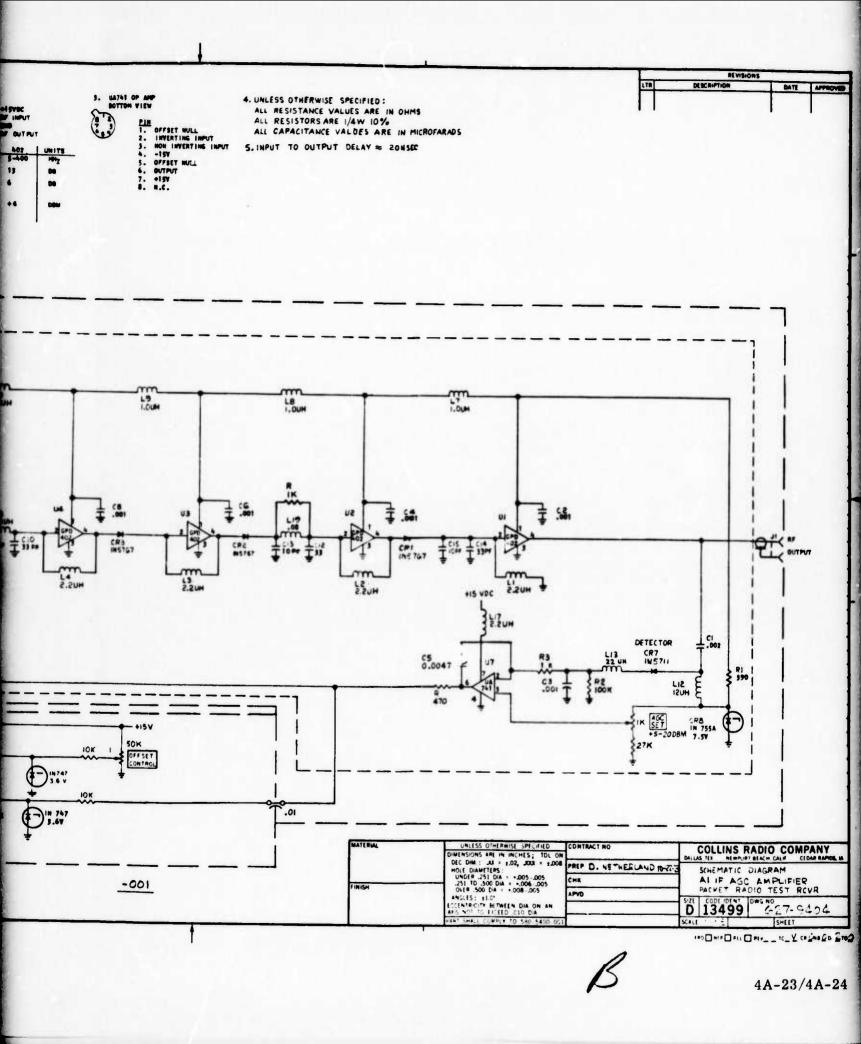


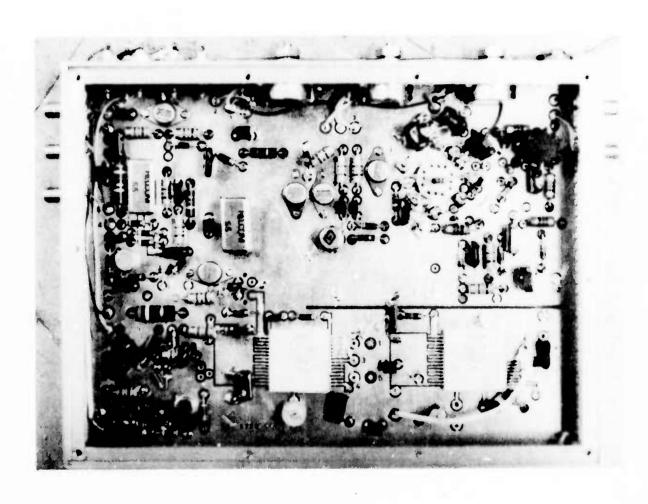


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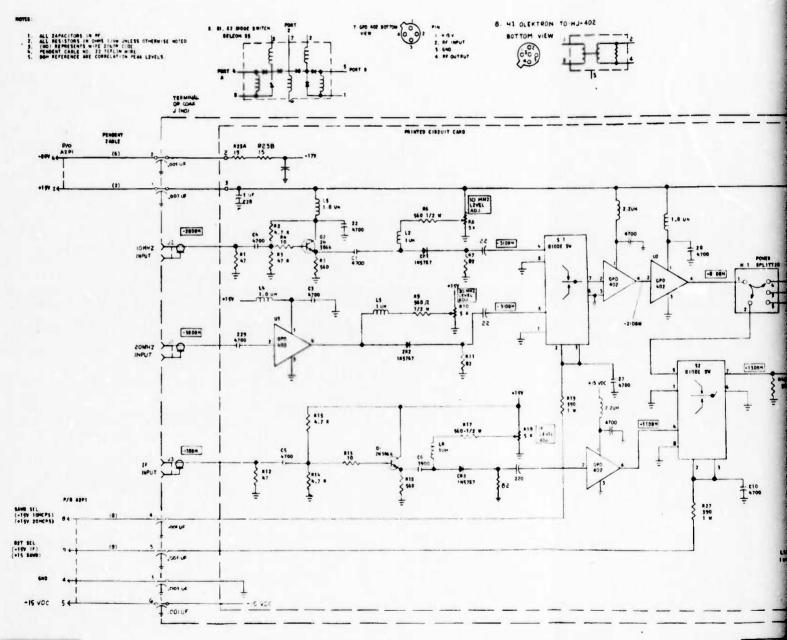






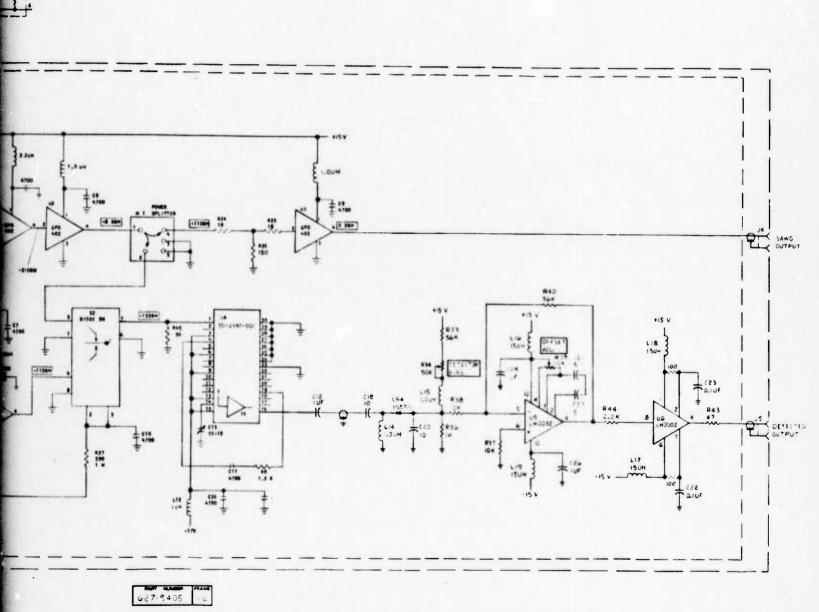


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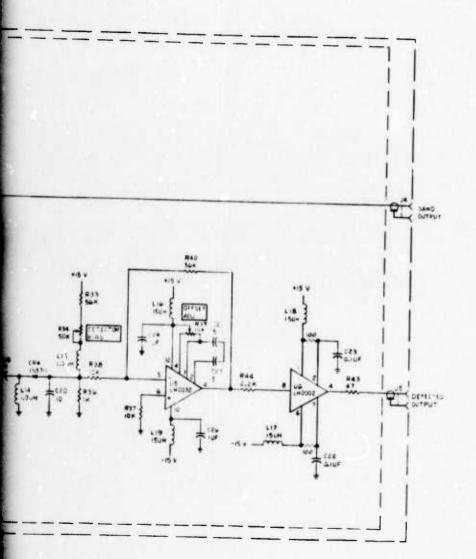
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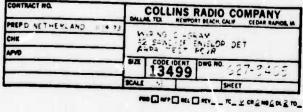
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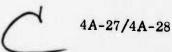


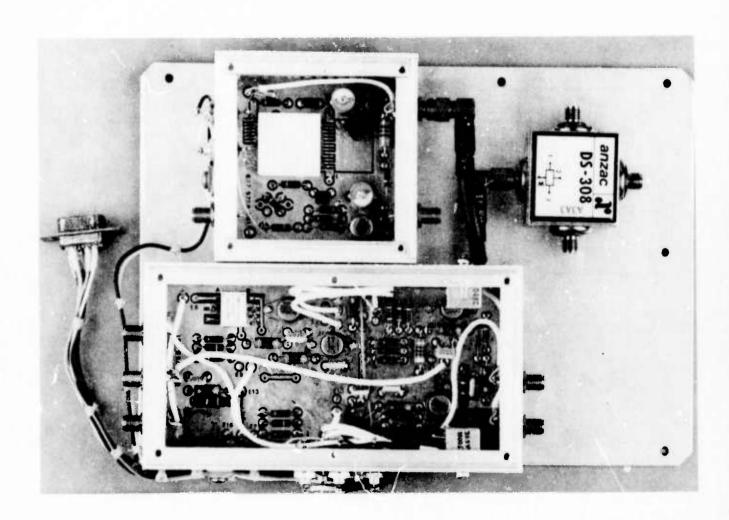
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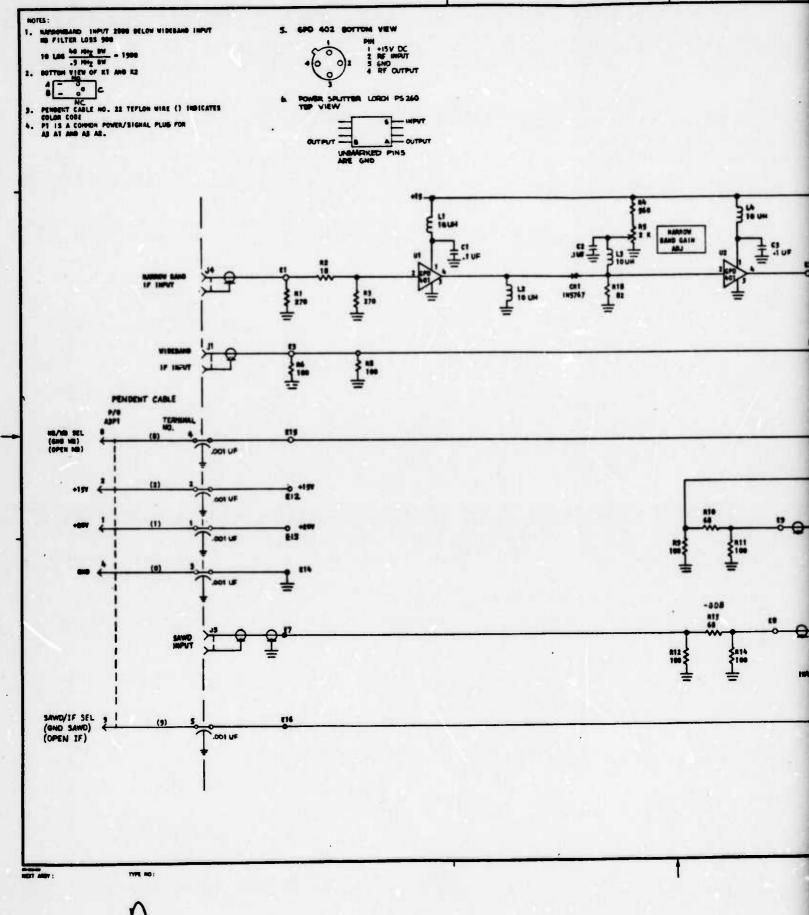


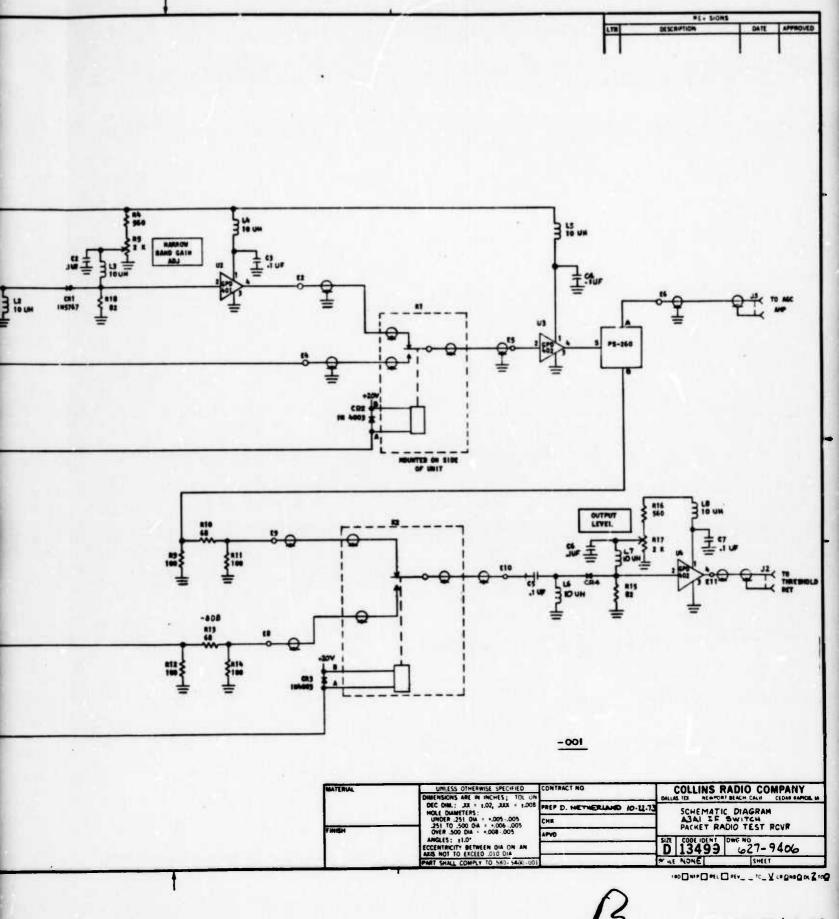




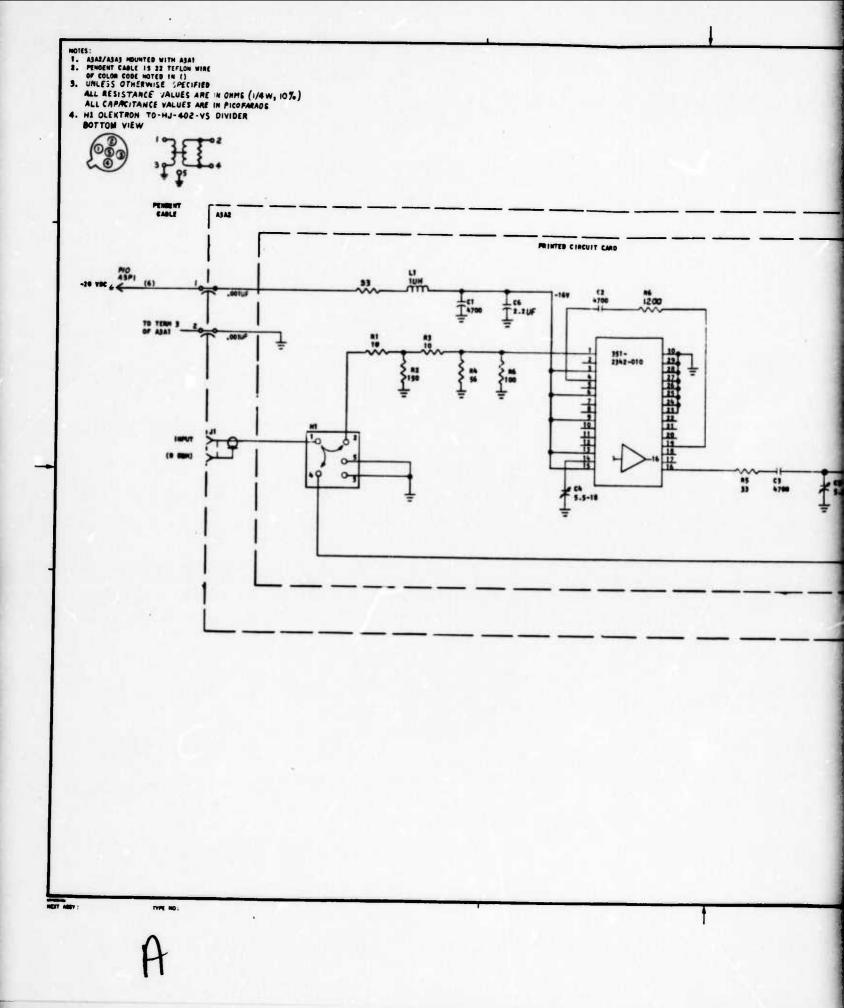


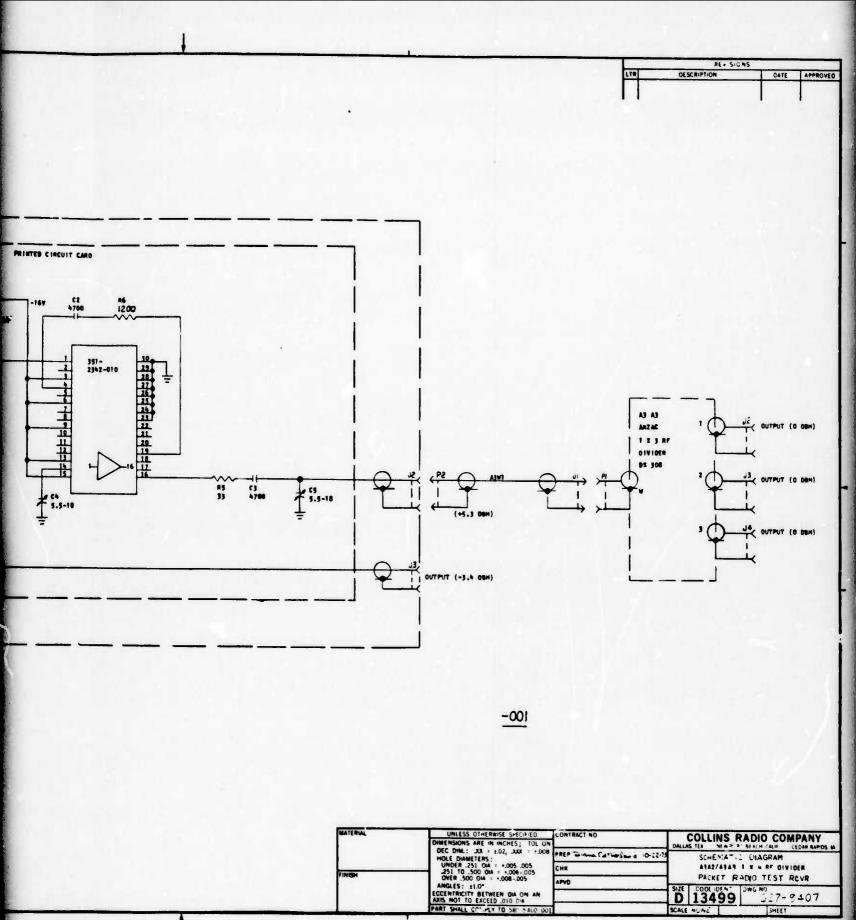






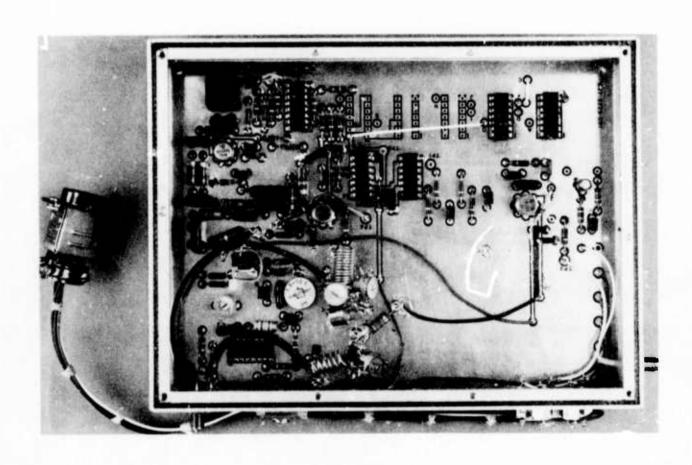
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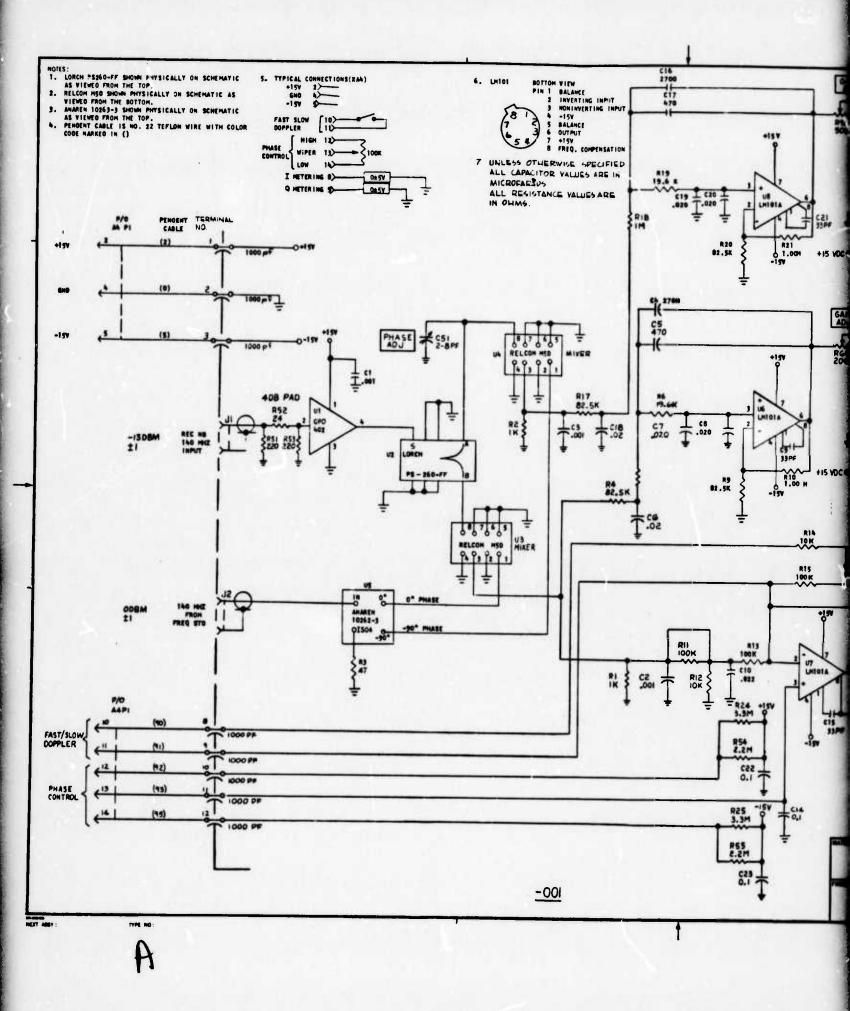


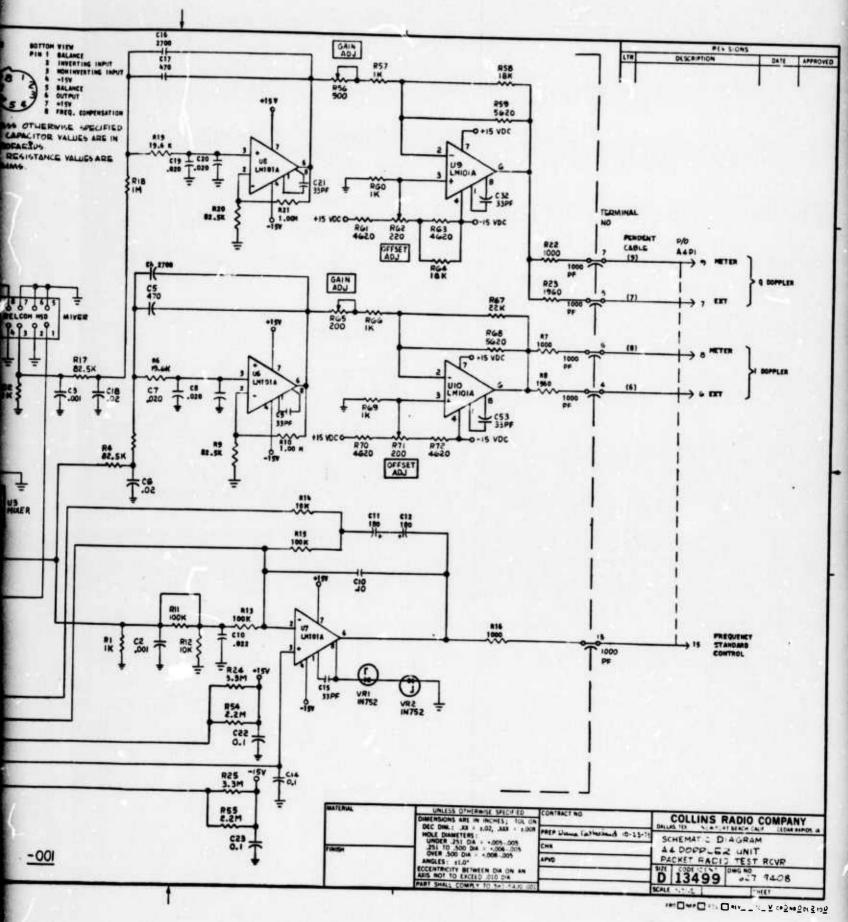


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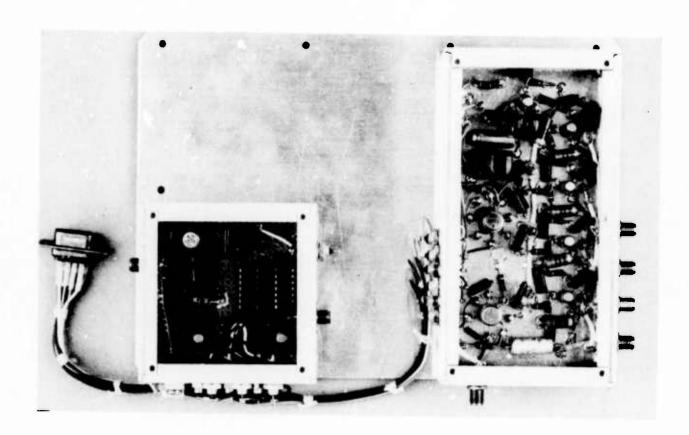
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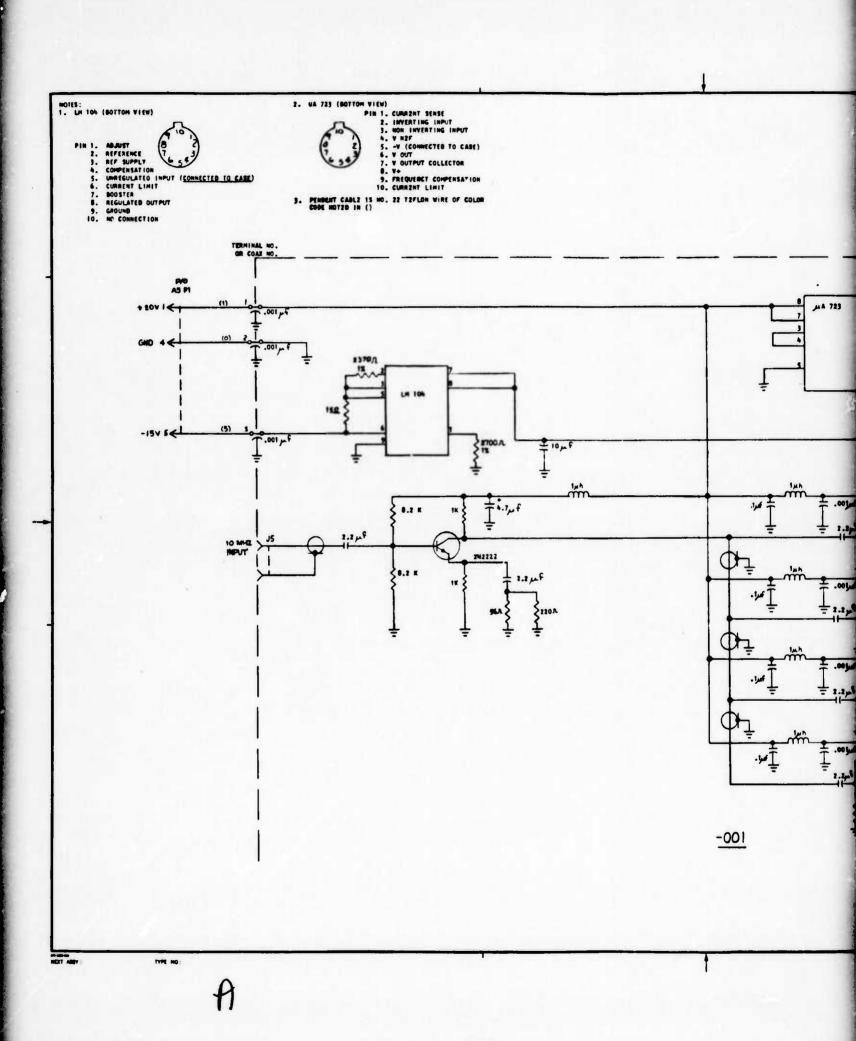


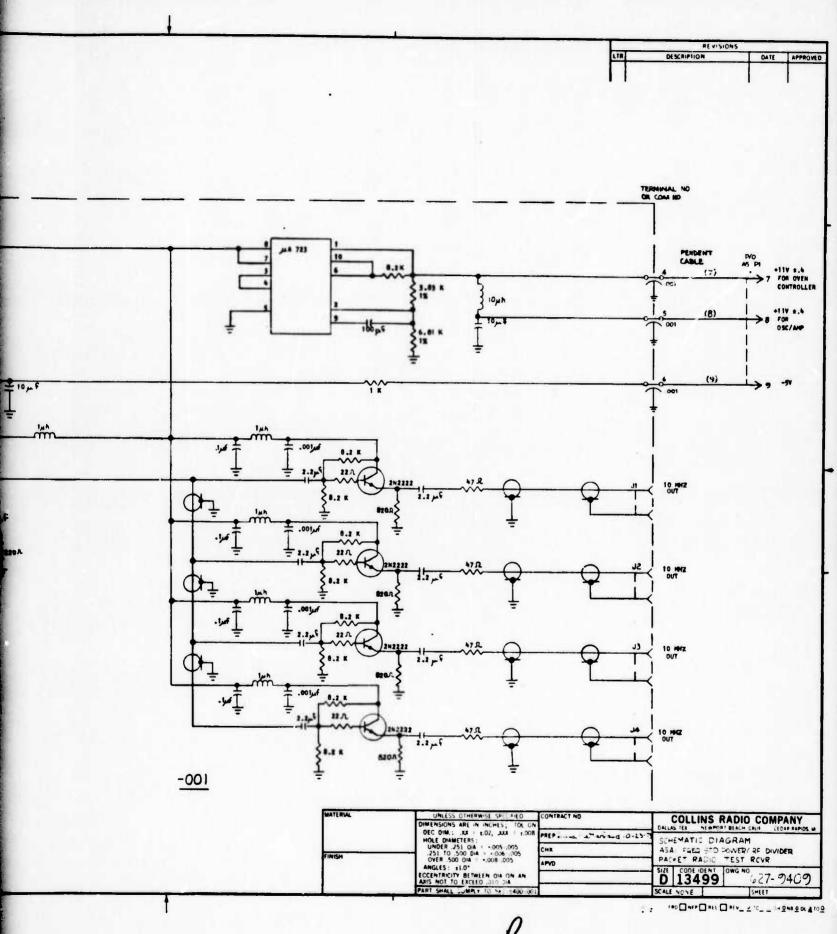


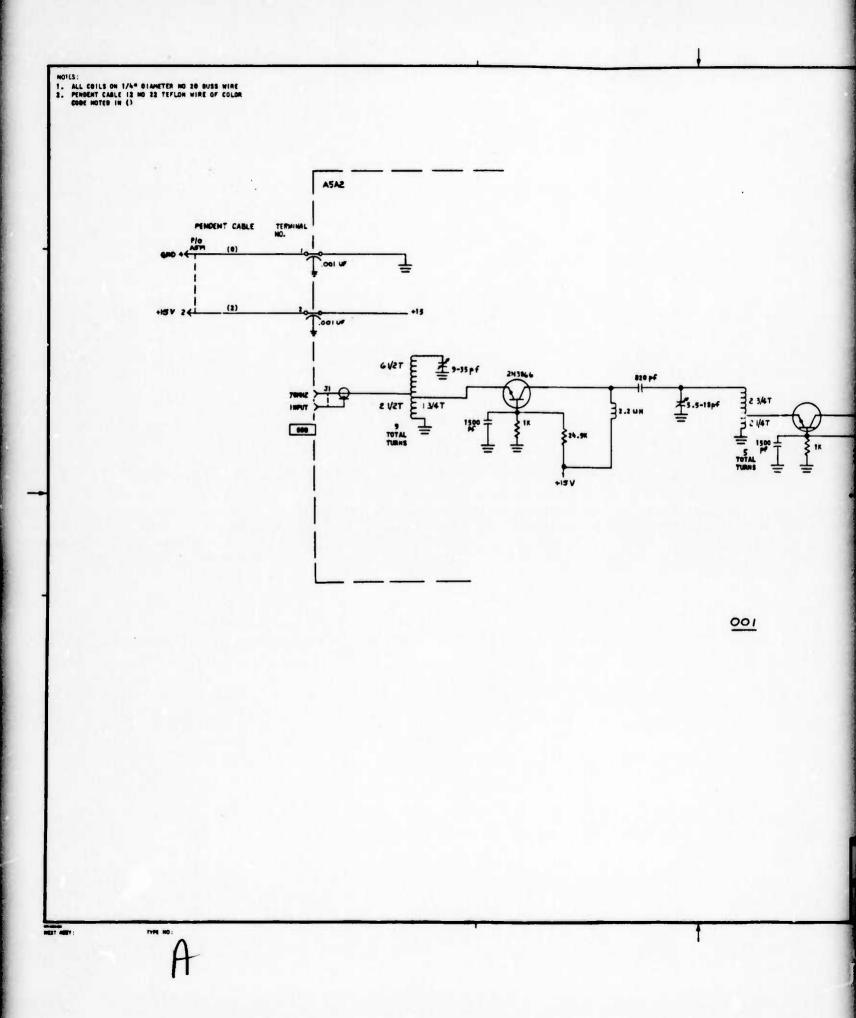


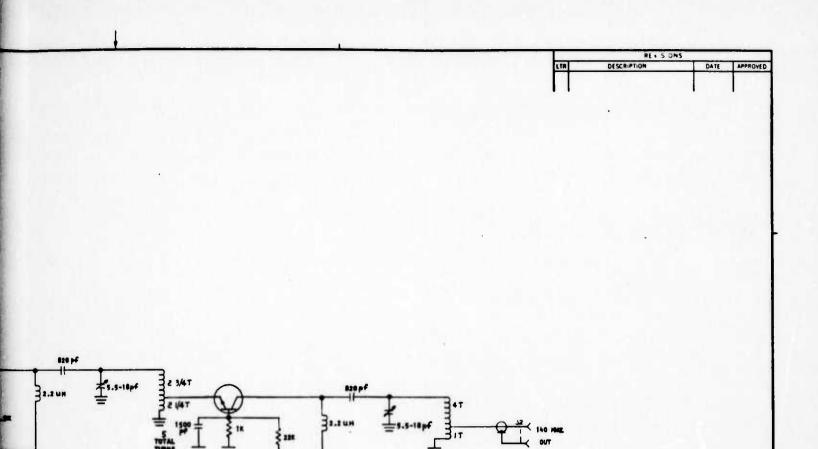
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DEC DIM.: JULY 2,02, JULY 1,008
HOLE DIAMETERS:
UNDER .251 DIA -.005 .005
JUNER .251 DIA -.005 .005
ANGLES: 11.0*

FINISH

DEC DIM.: JULY 2,02, JULY 1,008
HOLE DIAMETERS:
UNDER .251 DIA -.005 .005
OPER .500 DIA -.006 .005
ANGLES: 11.0*

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SCALL NONE

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DALLAS TEX N.E A-CHE RADIO COMPANY

SCHEMATIC DIAGRAM
AS AS MULTIPLIER X2
PACKET RADIO TEST REVR

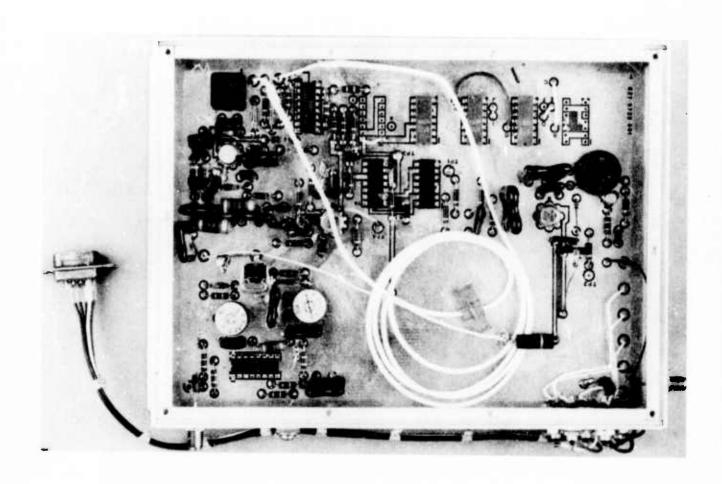
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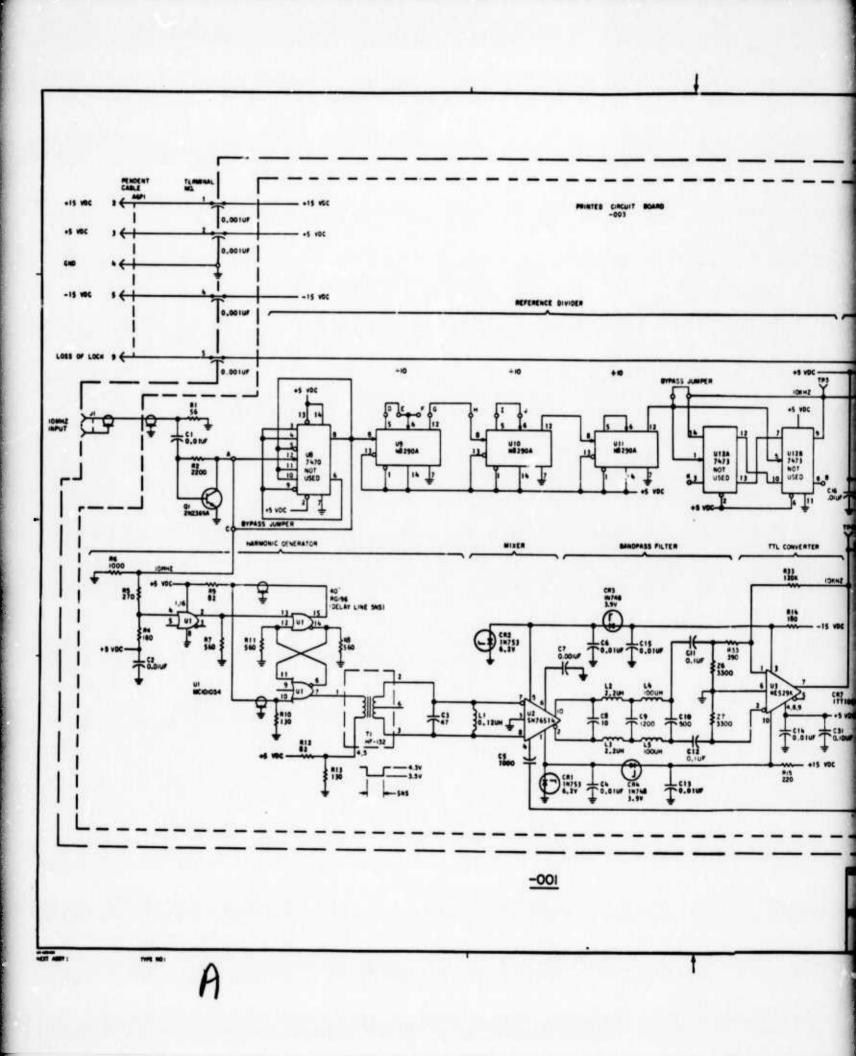
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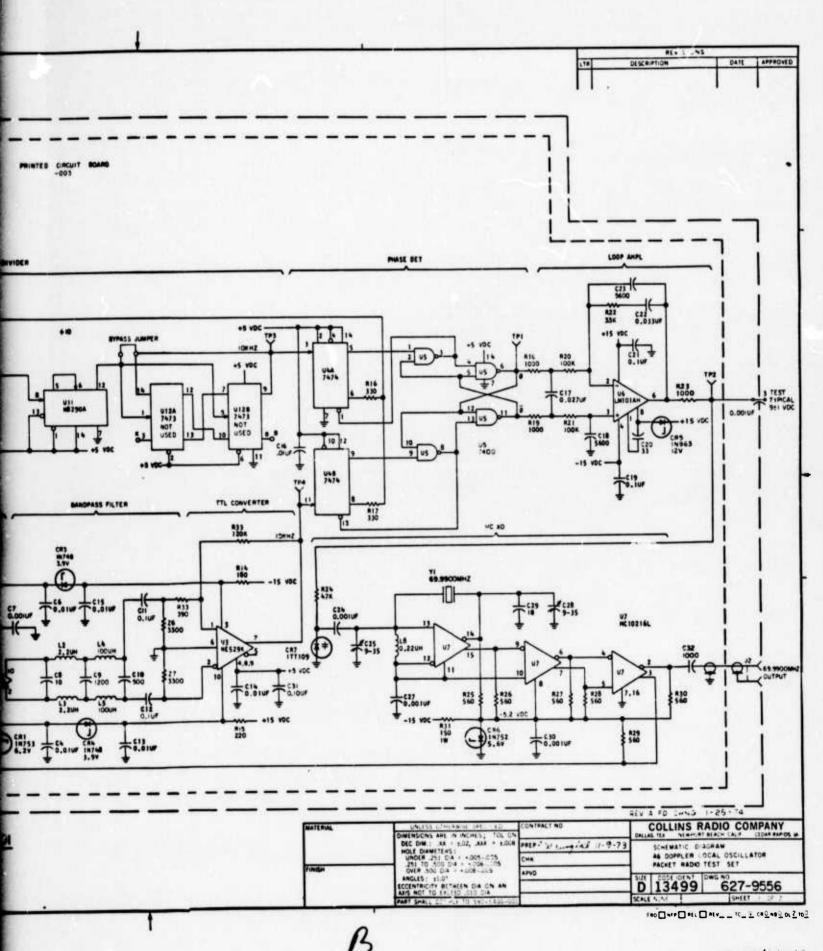
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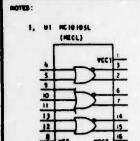
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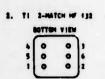


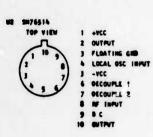
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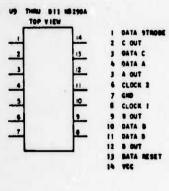


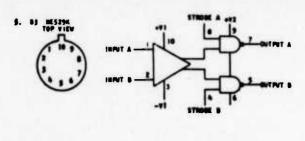


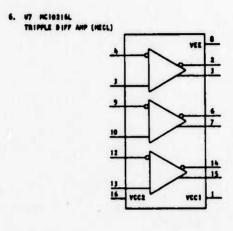


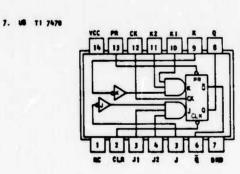


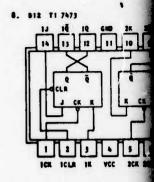


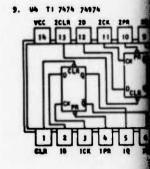


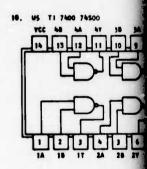










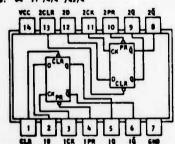


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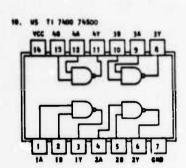
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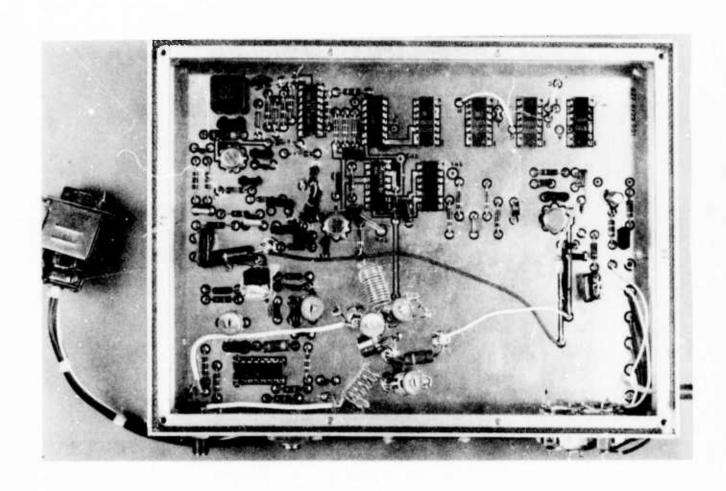


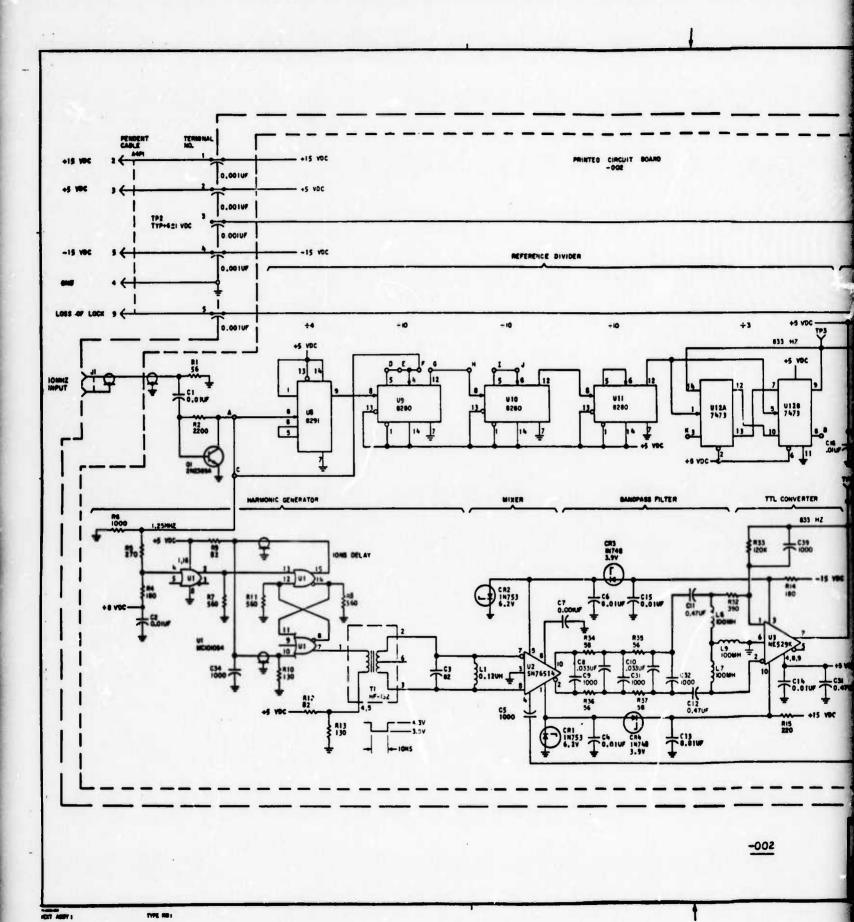
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ALL RESISTORS ARE 1/4 W CARBON
ALL CAPACITANCE VALUES ARE IN PICOPARABS.

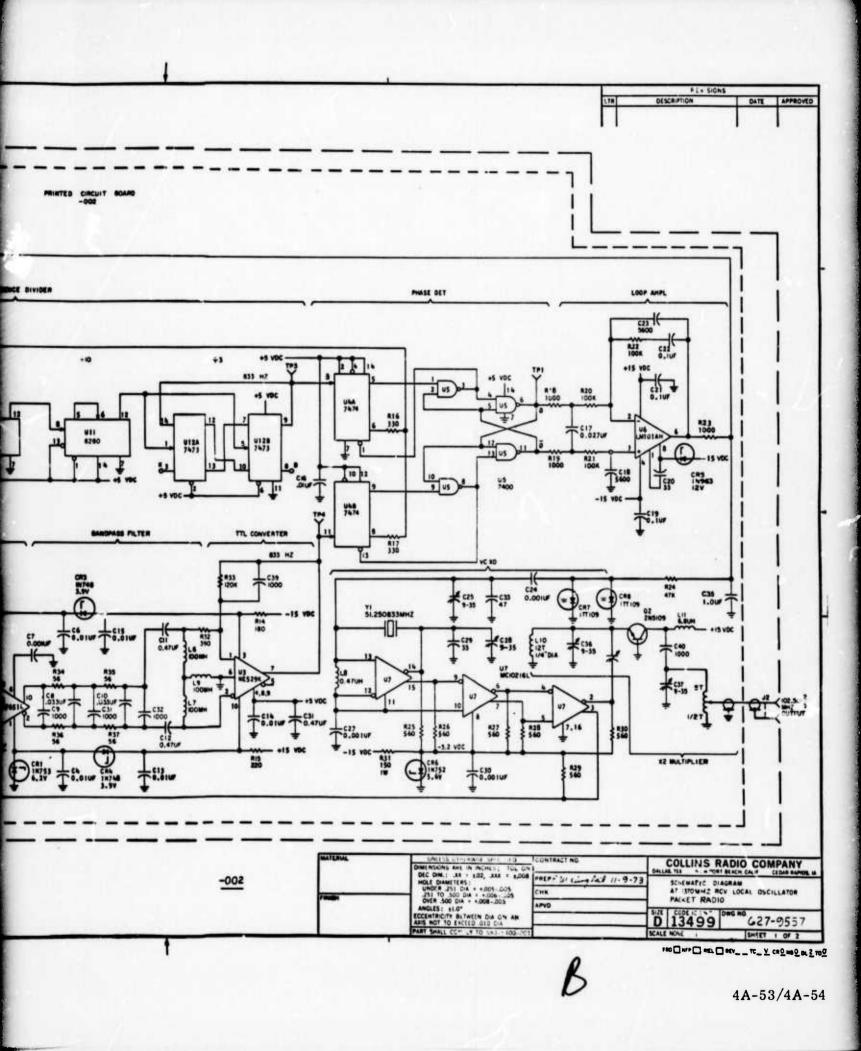


BIZE | CODE IDENT | DWG NO | 627-9556 | SCALE NONE | REV | SHEET | 2 OF 2



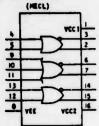












T1 2-MATCH HF 192

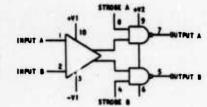


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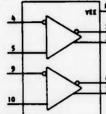


- 1 +VCC 2 OUTPUT FLOATING SHO
- LOCAL OSC INPUT -VCC DECOUPLE 1
- DECOUPLE 2
- . OUTPUT



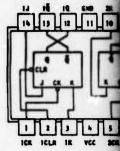


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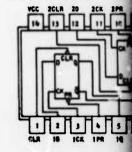
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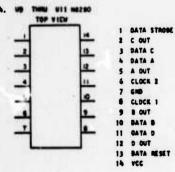
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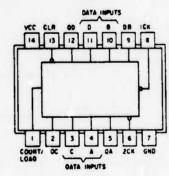
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9. 84 11 7474 74574

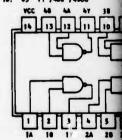




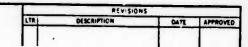
7. US NO291



18. US TI 7400 74500

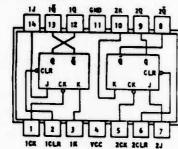




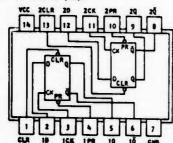


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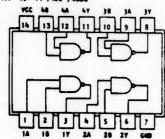


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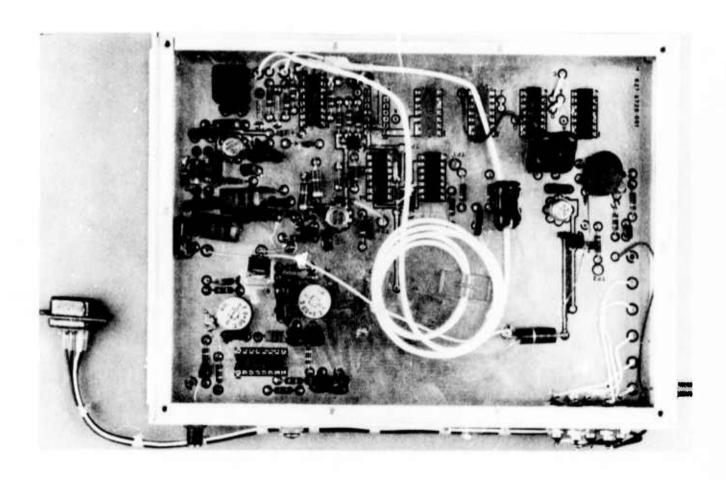
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ALL CAPACITANCE VALUES ARE IN PICOFARADS,



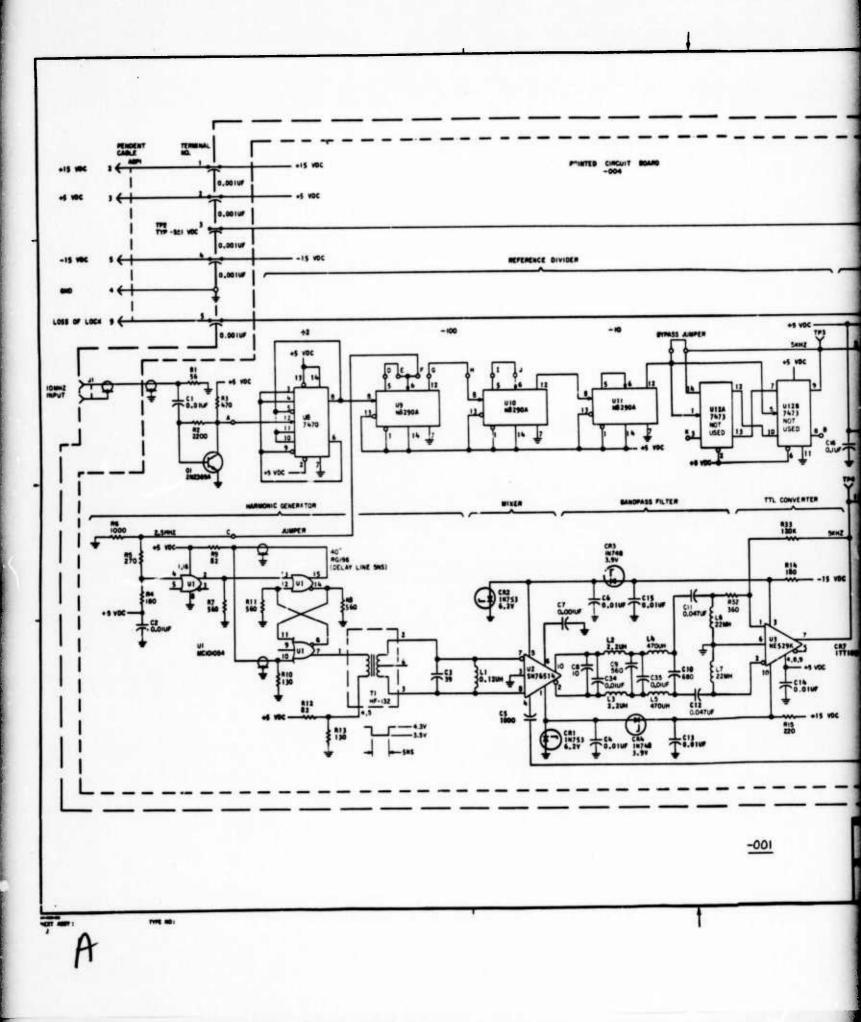


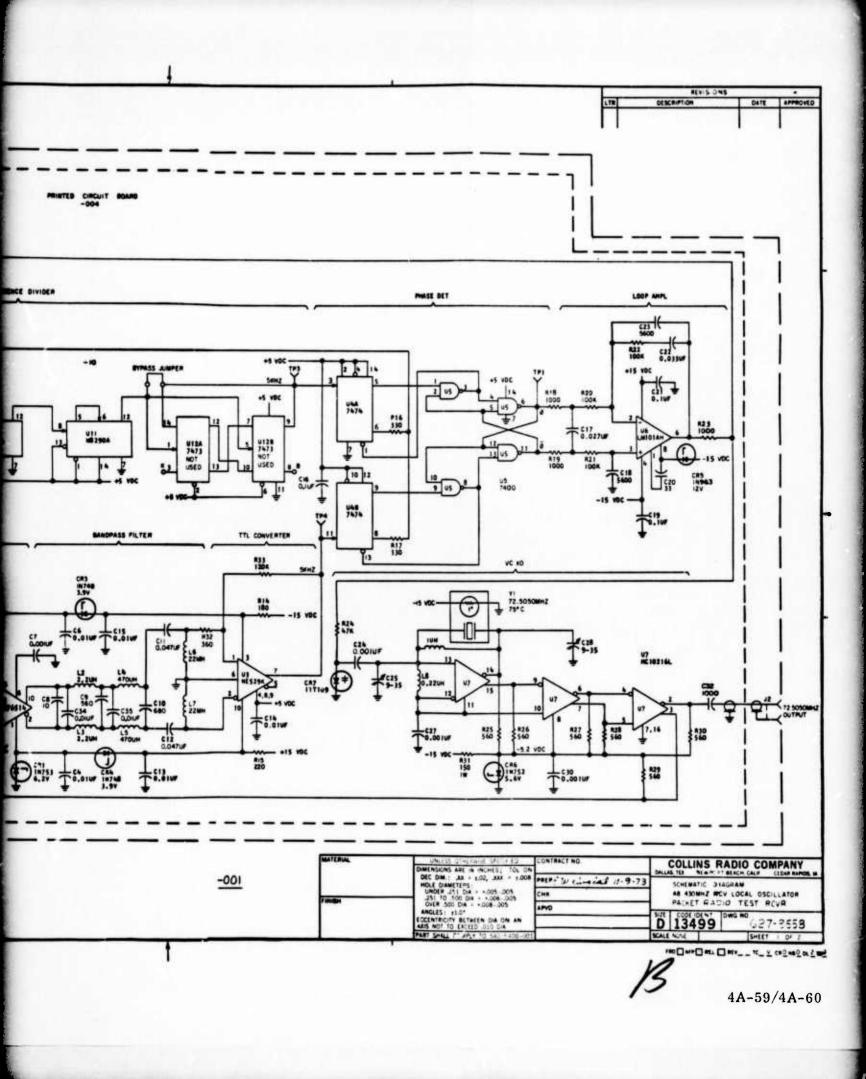
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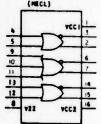
A8 - 430 MHZ RCV LO











2. TI 2-MATCH NF 132

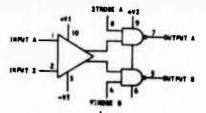


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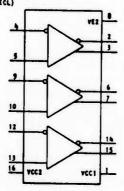


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- 3 FLOATING GIE LOCAL OSC IRPUT
- DECOUPLE 1
- OZCOUPLE 2 N INPUT
- 9 R C

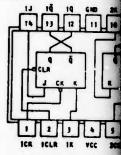




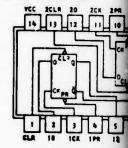
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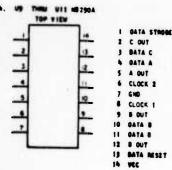


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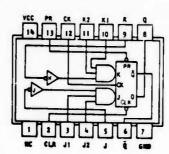
9. W T1 7474 /4574

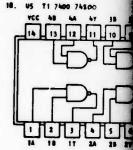


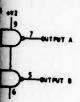


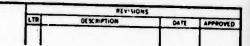
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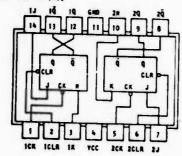




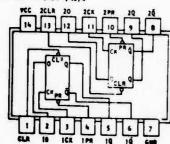




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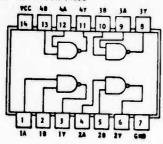


9. 44 11 7474 74574

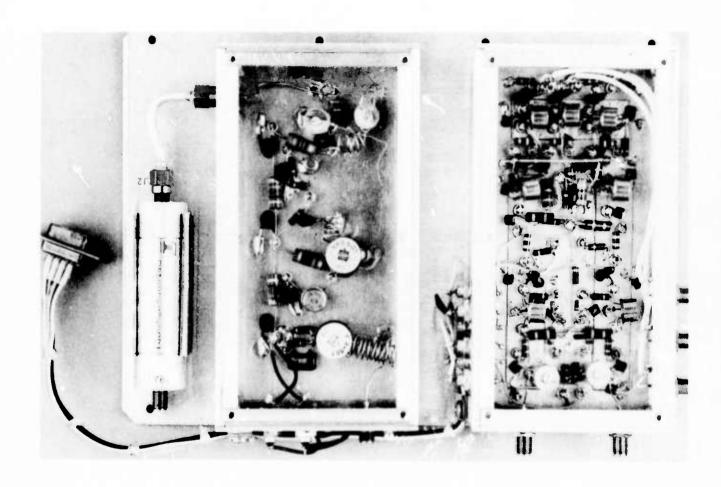


11. UNLESS OTMERWISE SPECIFIED
ALL RESISTANCE VALUES ARE IN OHMS
ALL RESISTORS ARE 1/4 W CARBON
ALL CAPACITANCE VALUES ARE IN PICOFARADS.

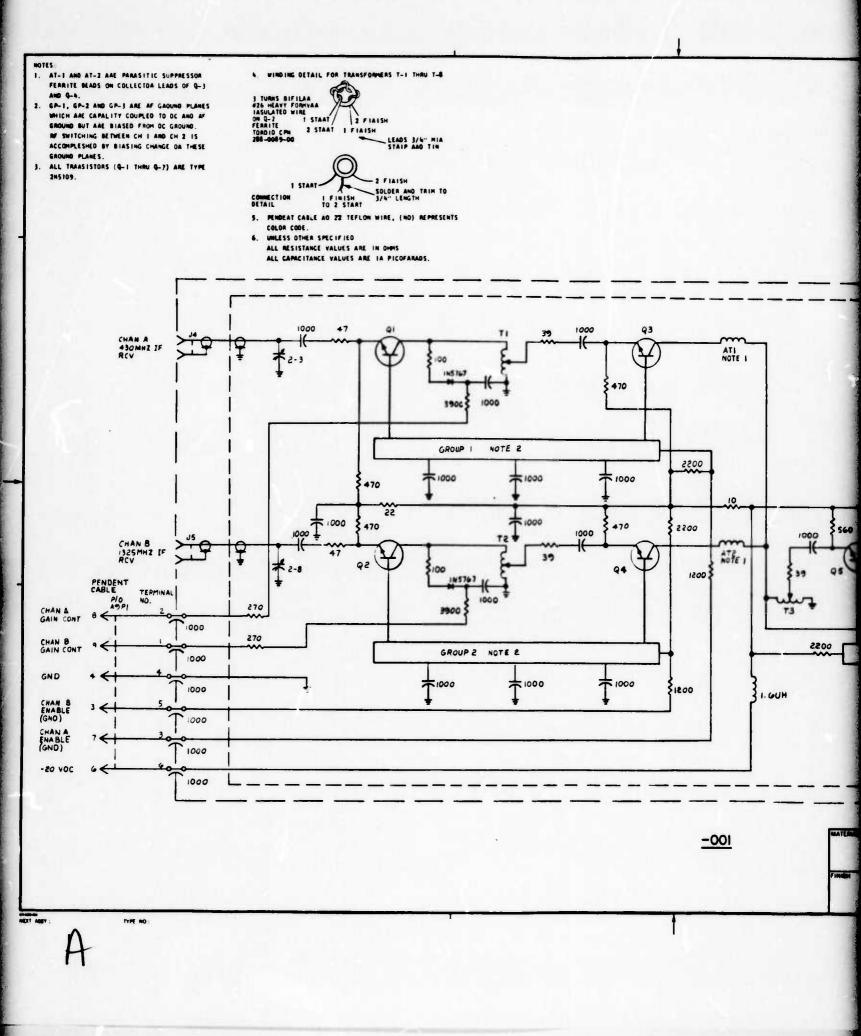
10. US TI 7400 74500

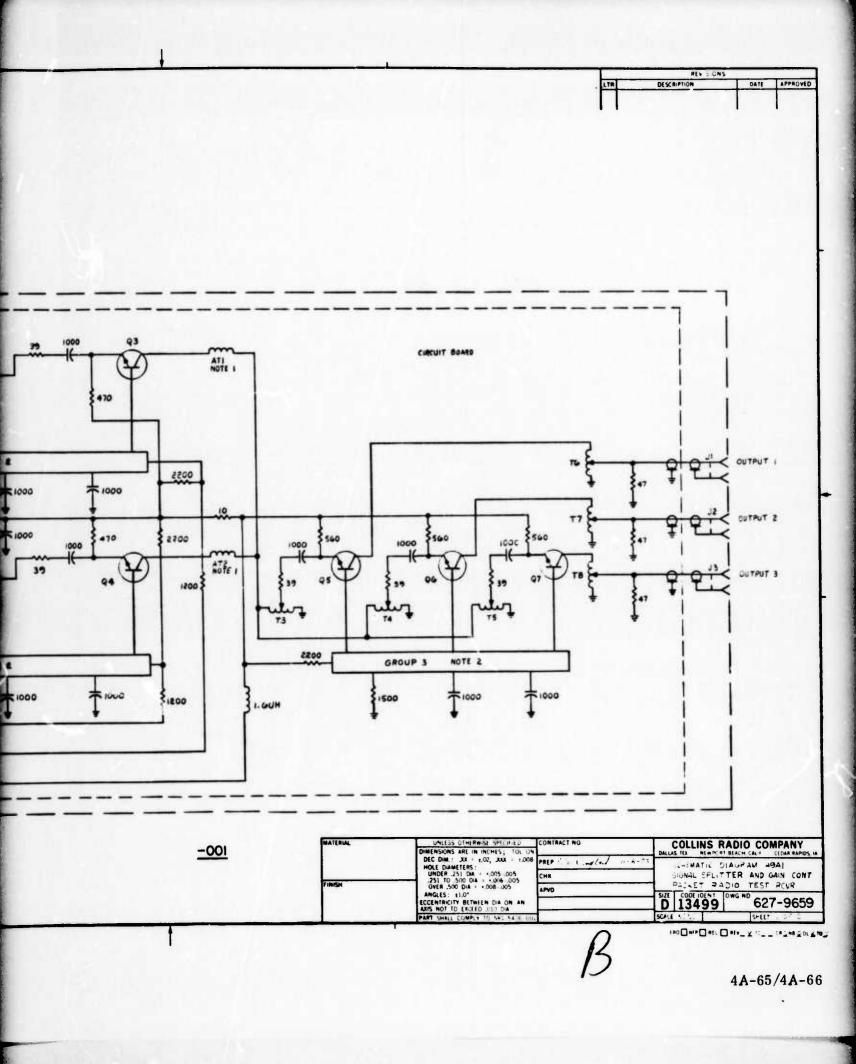


D 13499 027-3558



A9A1 - Signal Splitter/Combiner



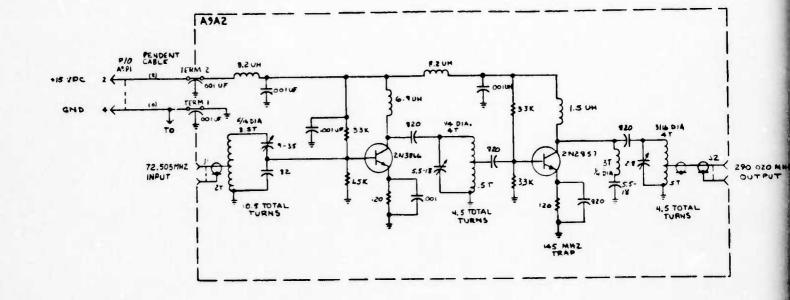


HOTES: I, COILS WOUND WITH #20 BUSS DIRE

2. PENDENT CABLE NO 22 TEFLON WIRE,

(NO) REPESENTS COLOR CODE

1. UNLESS OTHERWISE NOTED ALL CAPACITORS IN PROFARADS

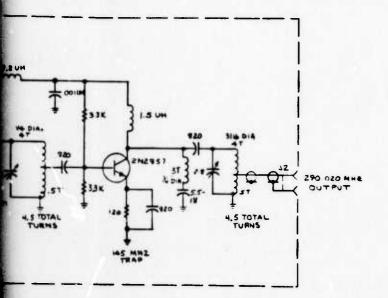


HELT ASEY:

TYPE NO

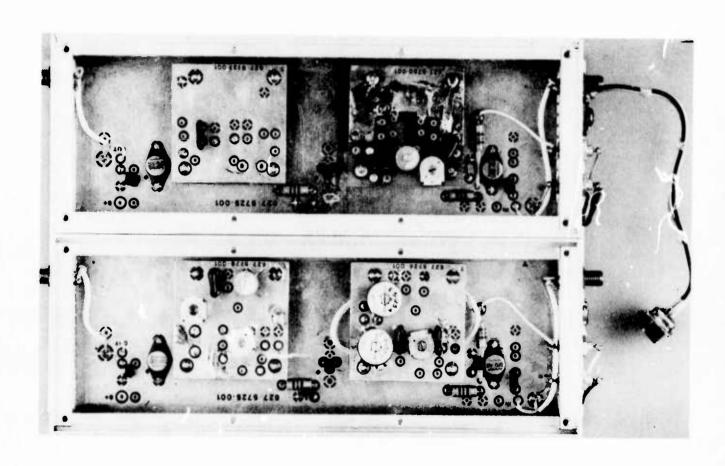
A

RE+ U ONS - DESCRIPTION APPROVED DATE



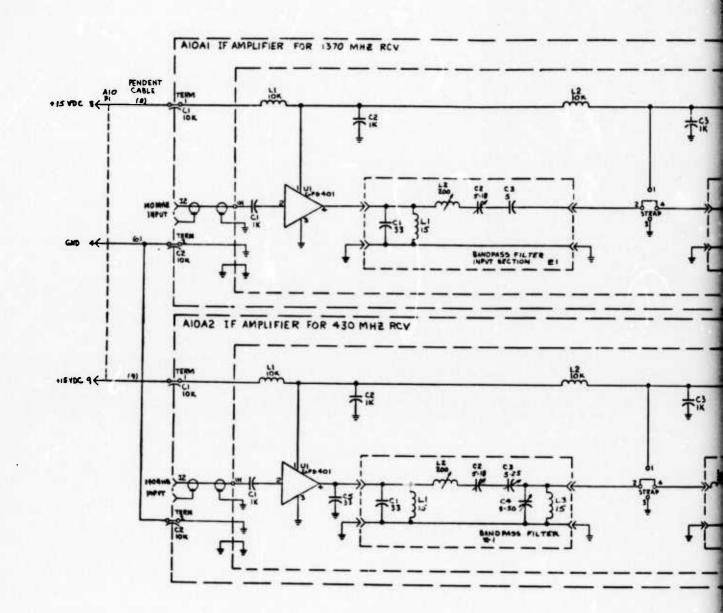
UNLESS CHERRISE SPENT ED
DIMENSIONS ARE IN INCHES; TOL ON
DEC DIM.: JAX = 1,02; JAX = 1,008
MOLE DIAMETERS:
UNDER 251 DIA = 1,005.005
251 TO 3500 DIA = 1,006.005
DVER 3500 DIA = 1,006.005
ANGLES: 11.0*
ECCENTRICITY BETWEEN DIA ON AN
AXIS NOT TO EXCEED 110 DIA
PART SMALL CO* PLY TO 580 5400 C. COLLINS RADIO CO MPANY PREP. TOUY FITE 3-11-73 AMING DI-GRAM ARAS MULTIPLIER X4 PACKET HAPIO TEST POUR SIZE CODE IDEN | DWG ND | 627-9659 APVD SCALE N. V.

FRO NEP OE _ DEV__1C_ Z CR_NO 2 DE 2 102



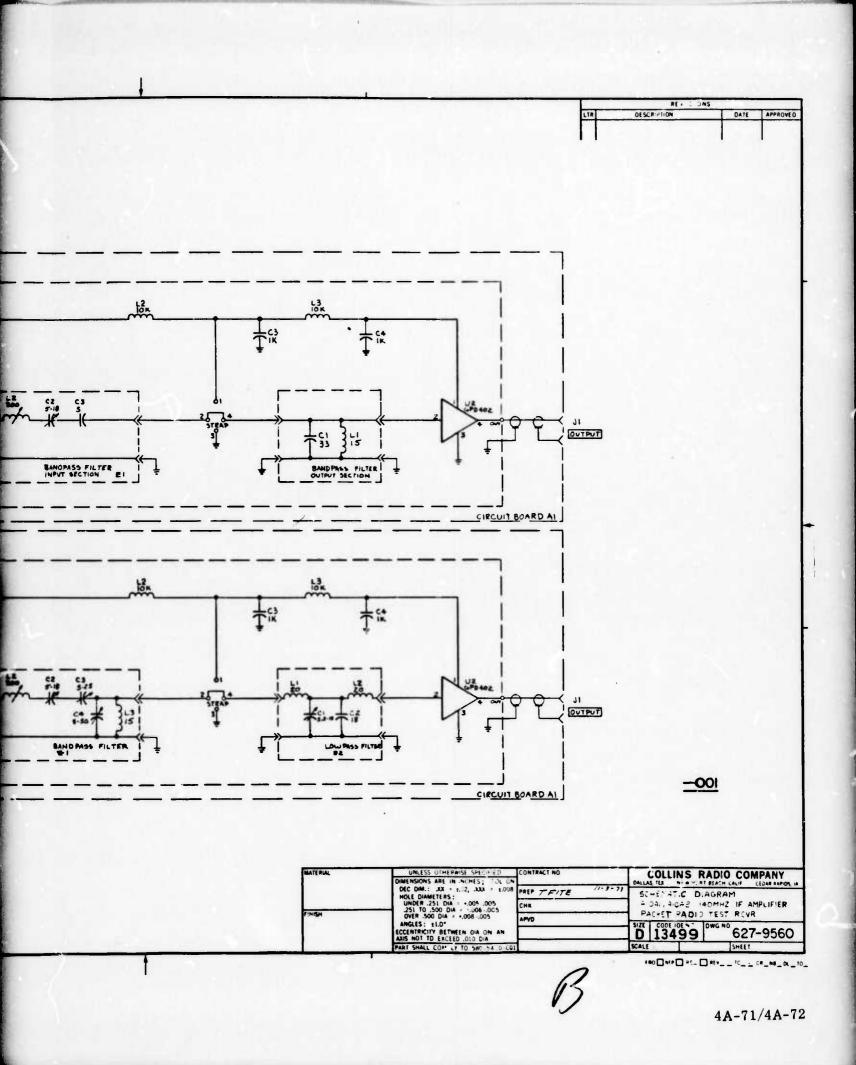
NOTES:

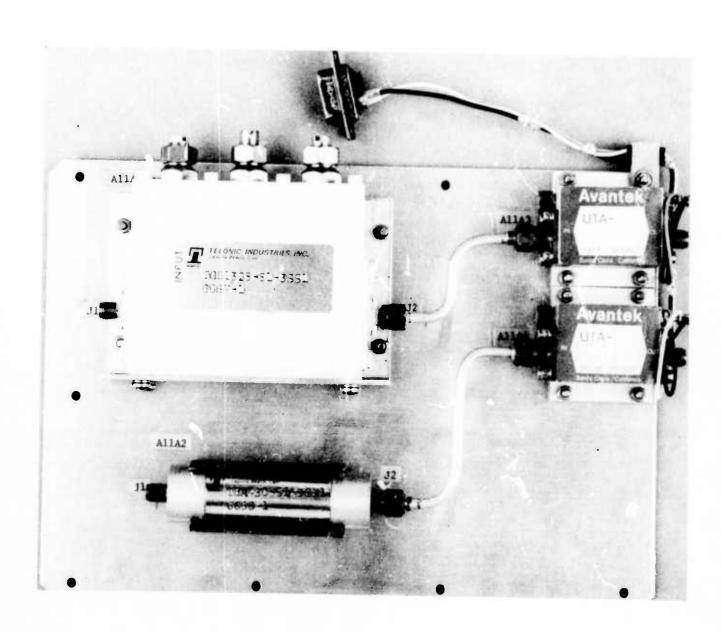
- I. ALL CAPACITORS ARE IN PF & ALL INDUCTORS ARE IN UH 3. GPD 401/402 BOTTOM VIEW
- 1. HIS VDC 2. RF INPUT 3.GND 4. RF OUTPUT
- 4. PENDENT CABLE NO. 22 TEFLON WIRE. (NO) REPRESENTS COLOR CODE.



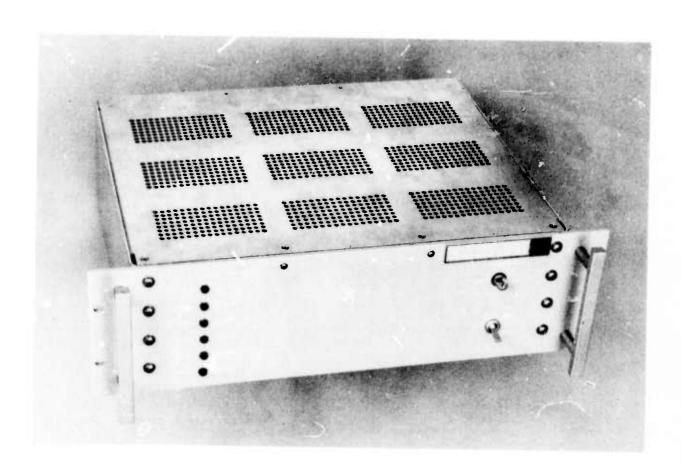
HEXT ASSY:

-

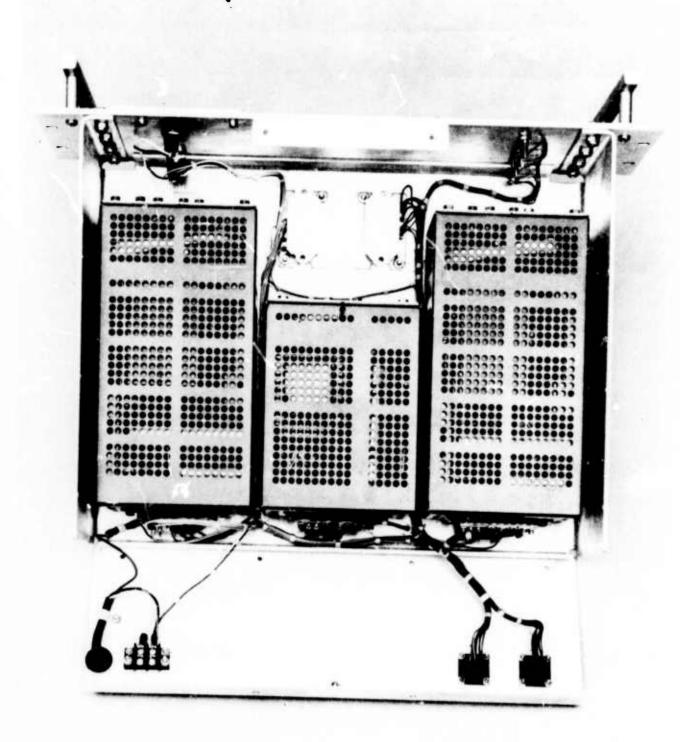




A11 - RF AMPL & FILTER



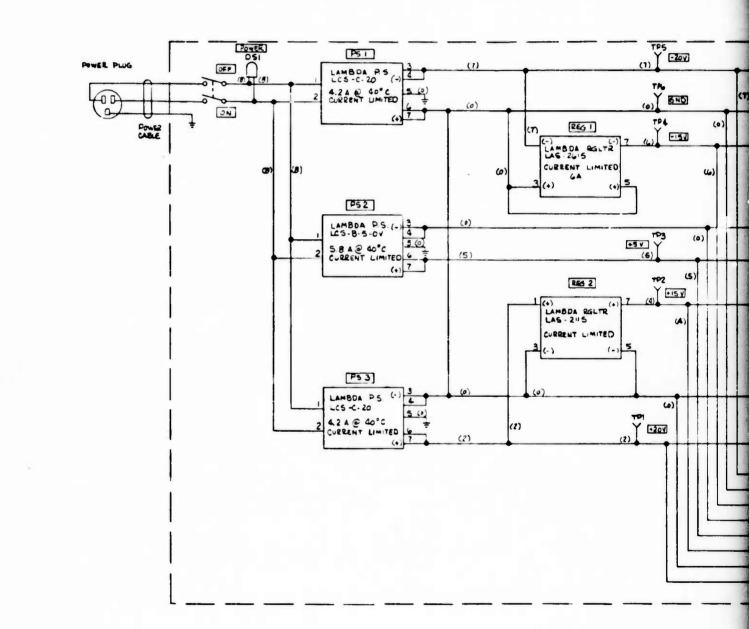
Front View



Internal Assy

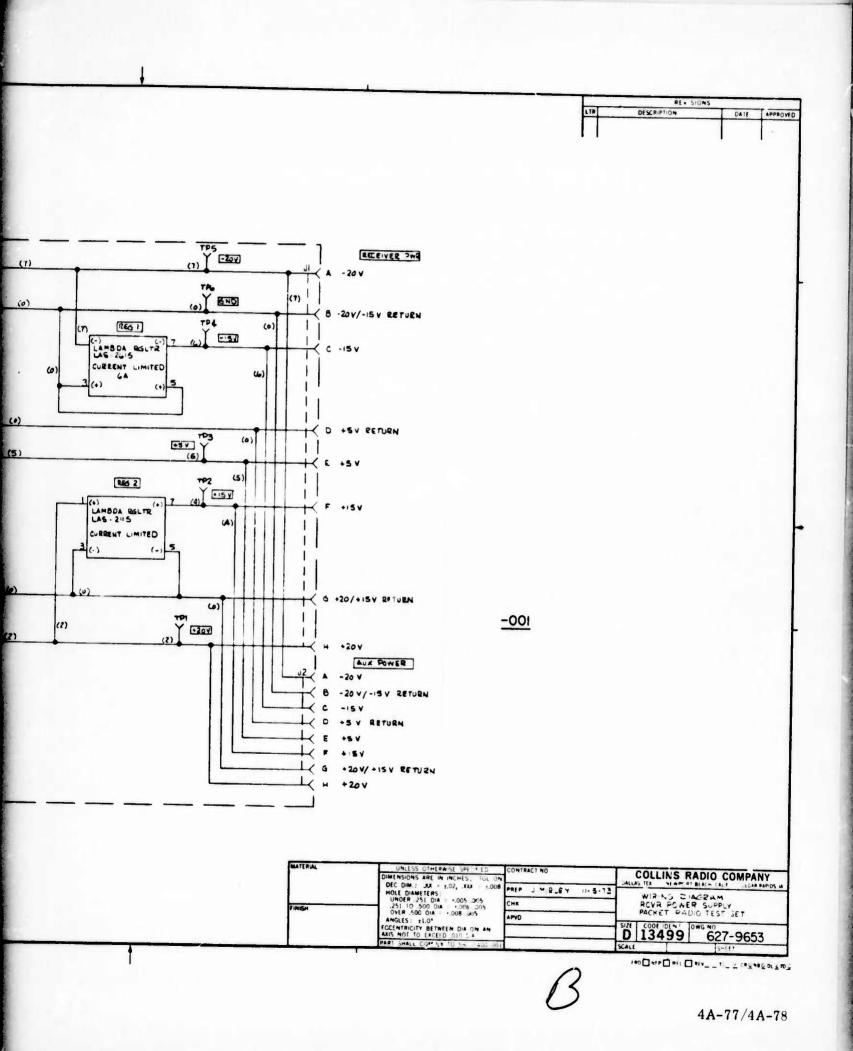
NOTES.

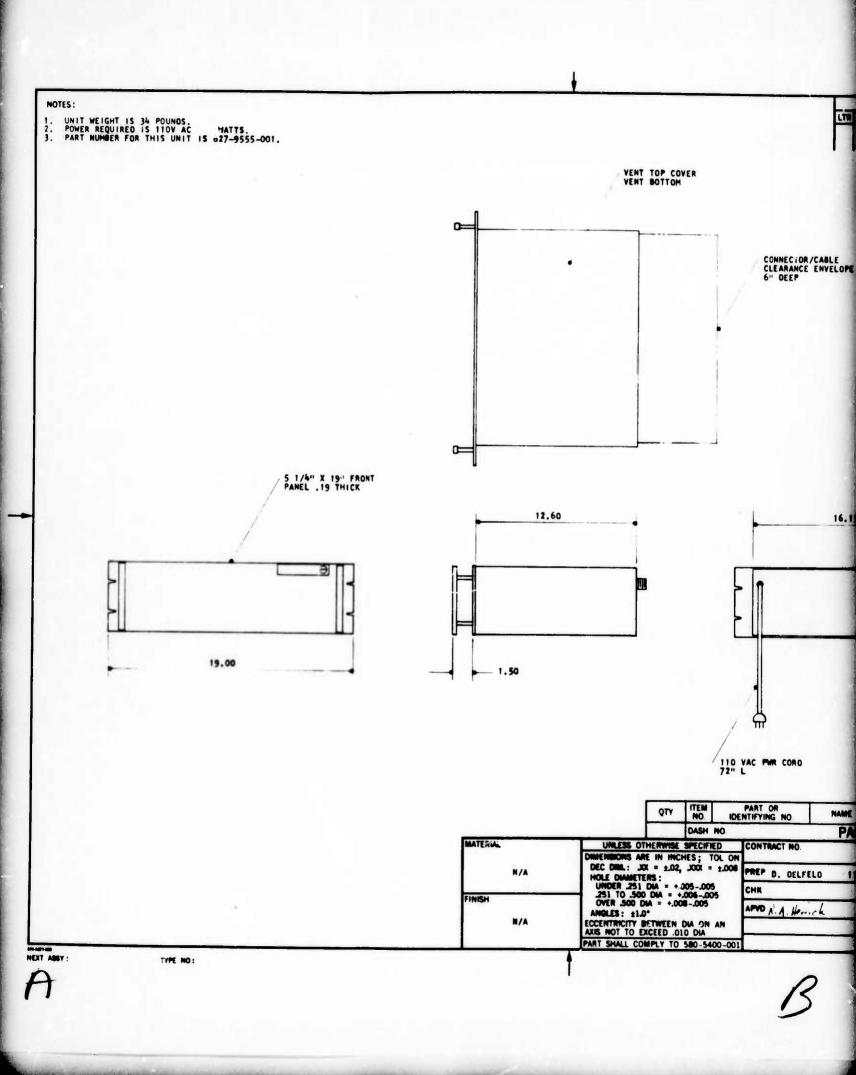
- I. ALL CHASSIS ITEMS TO BE IDENTIFIED BY BUBBER STAMP OR OTHER MEANS ON CHASSIS.
- 2. NO 20 TEFLON AIRE TO BE JOED JULESS CTHERWISE MOTED. (X) INDICATE WIRE COLDR 1008.

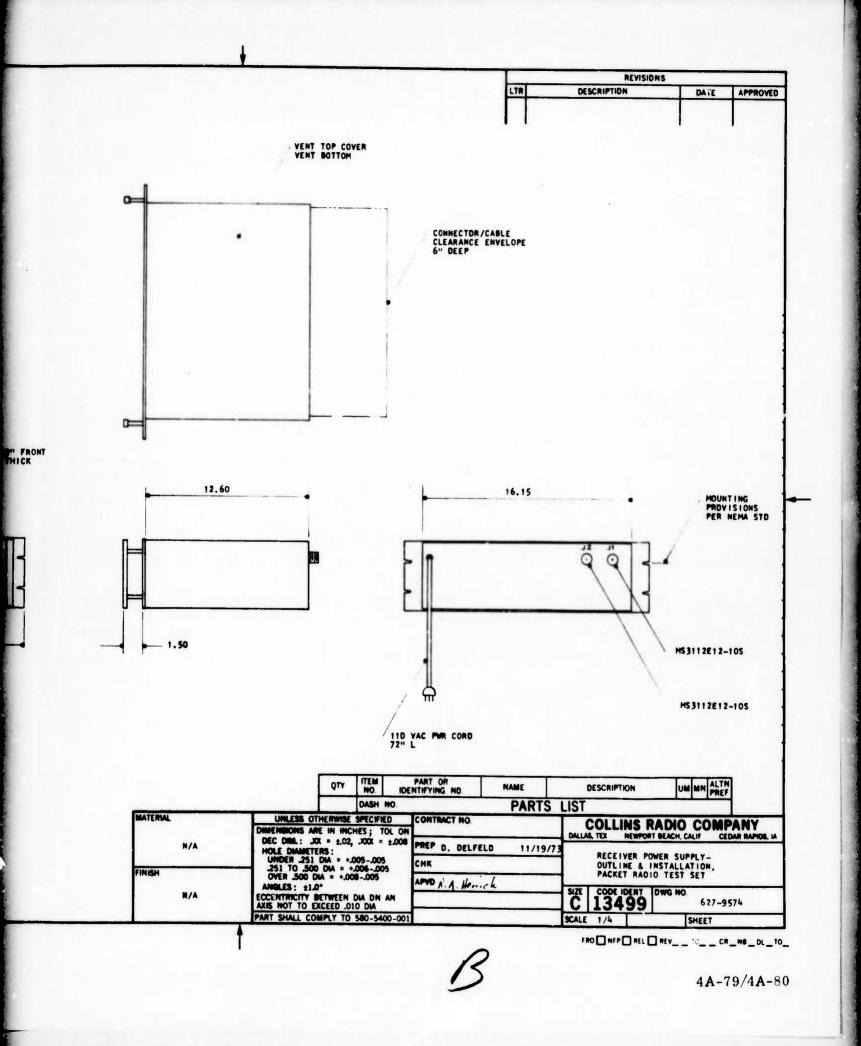


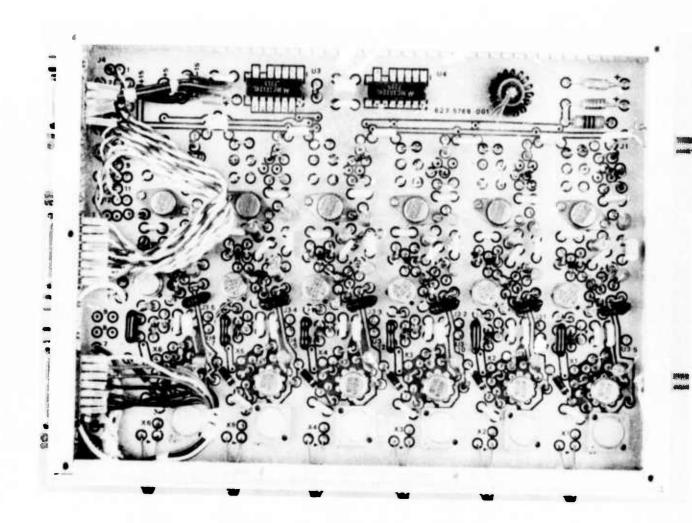
A

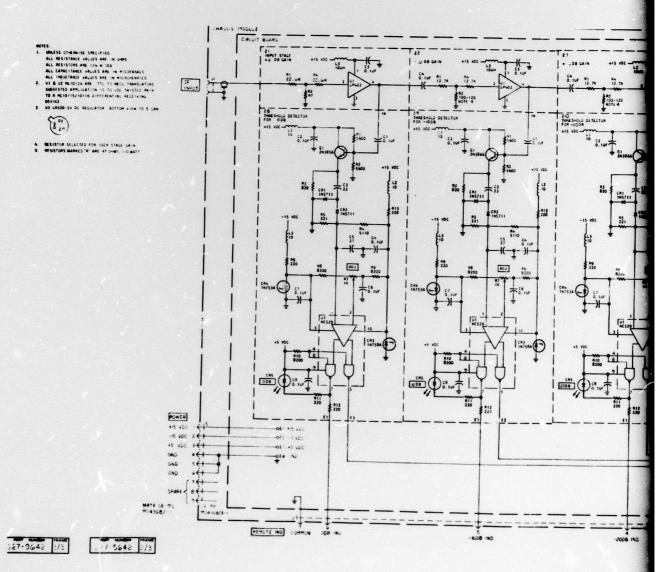
TYPE NO



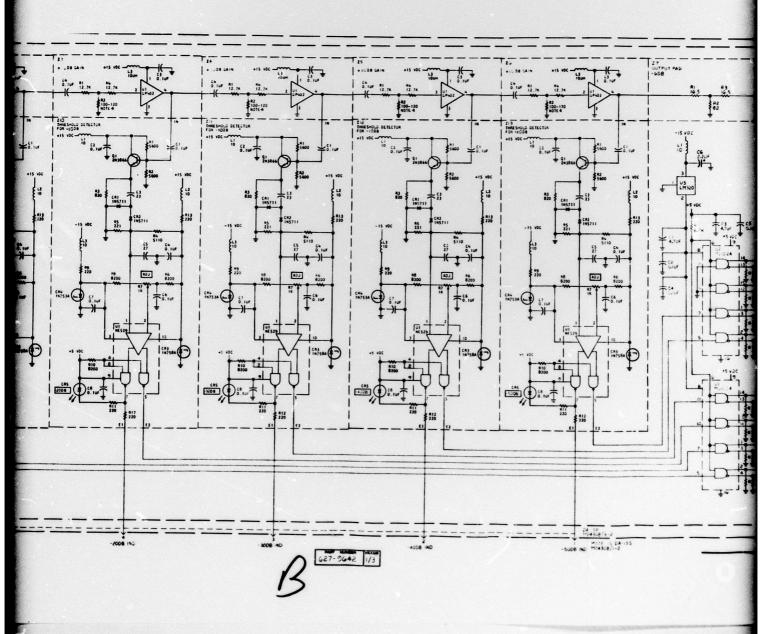


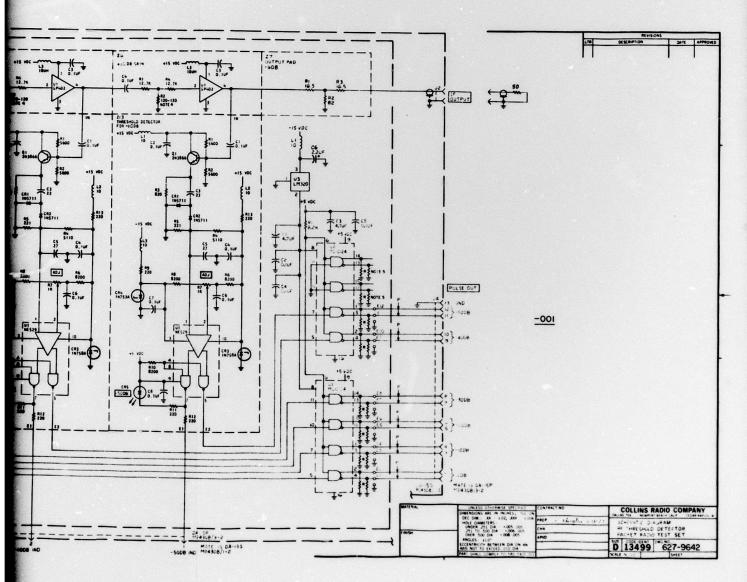






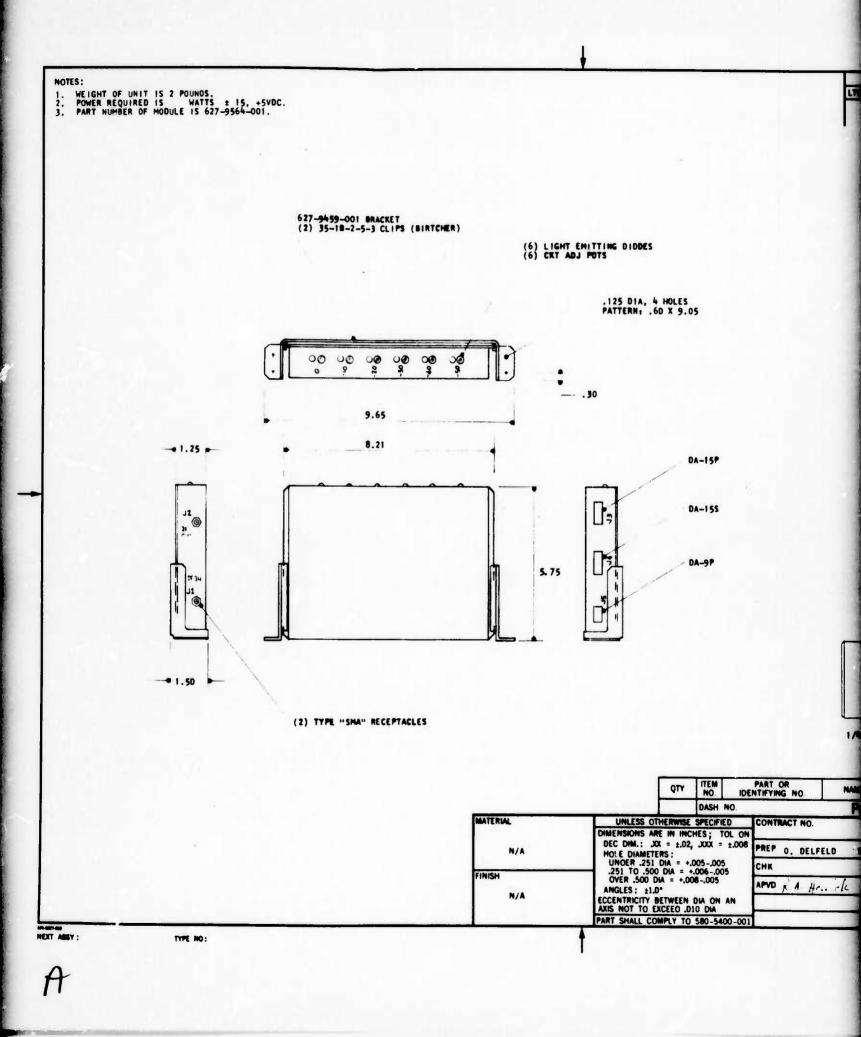


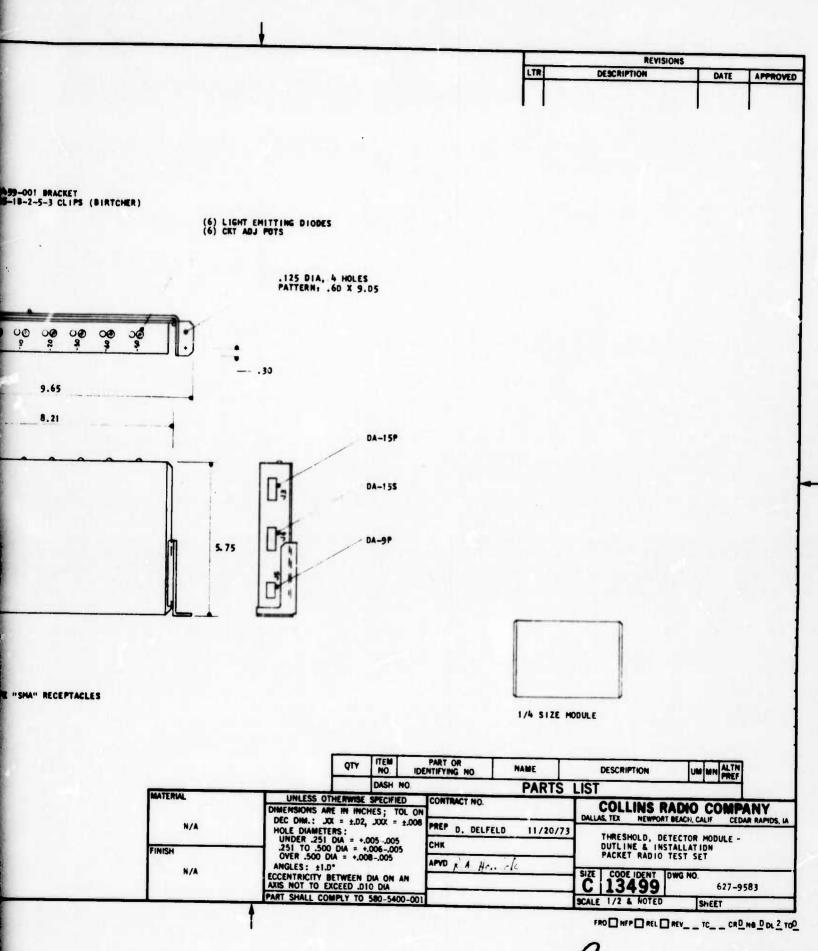




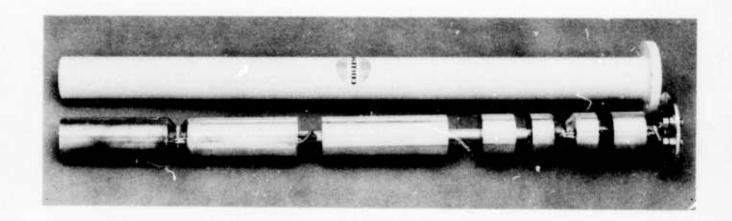
0

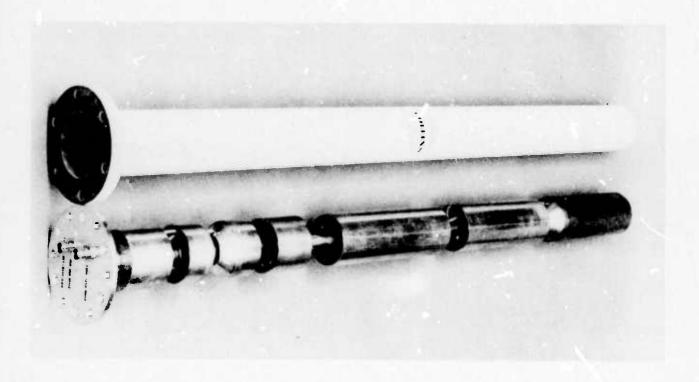
4A-83/4A-84



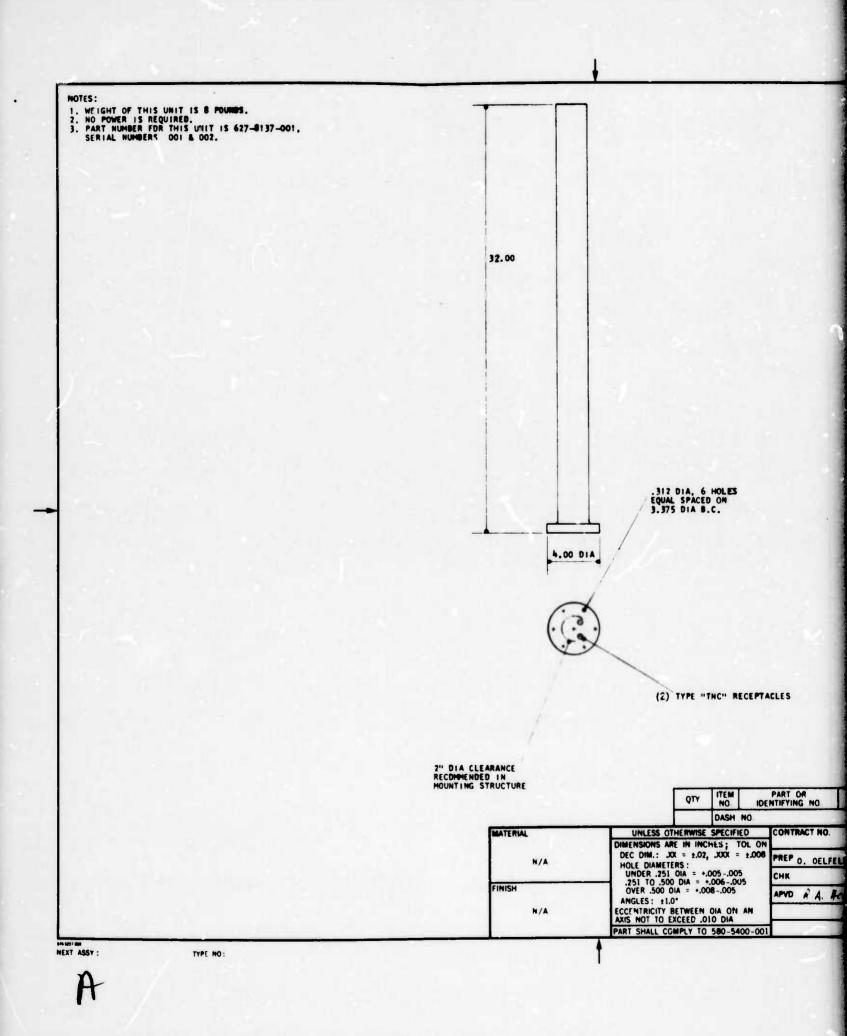


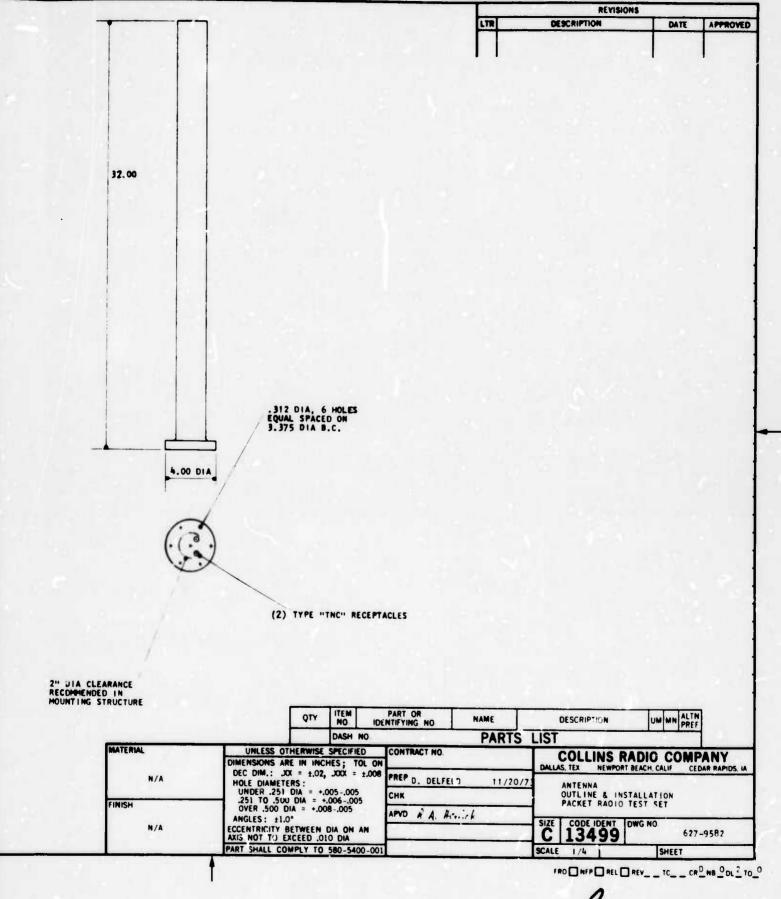
13





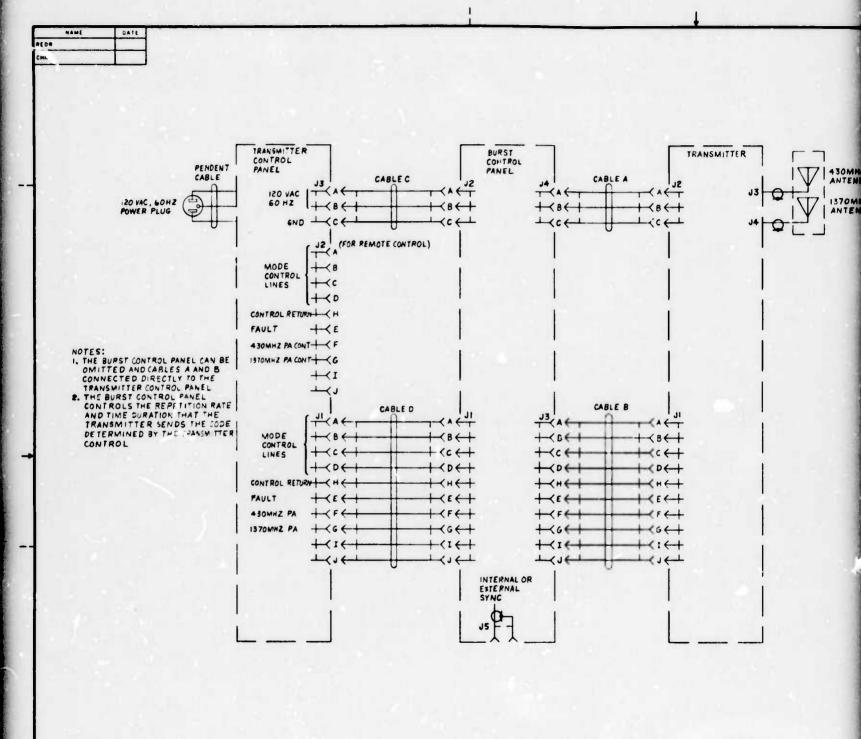
Assembly

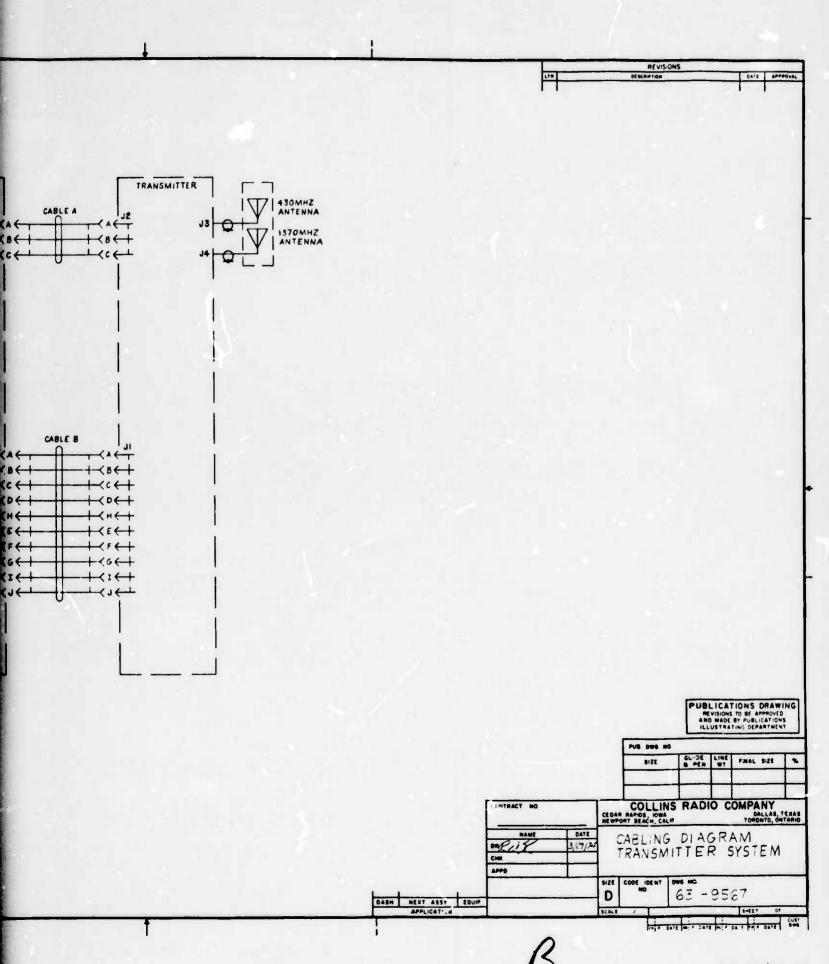


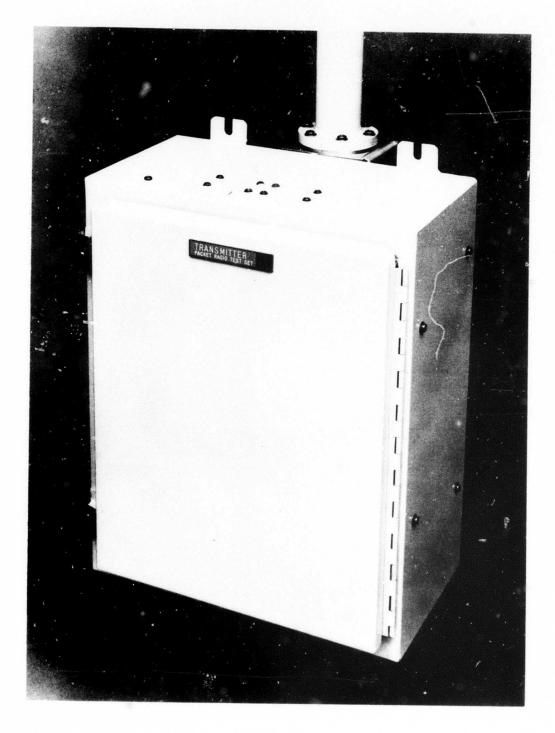


B

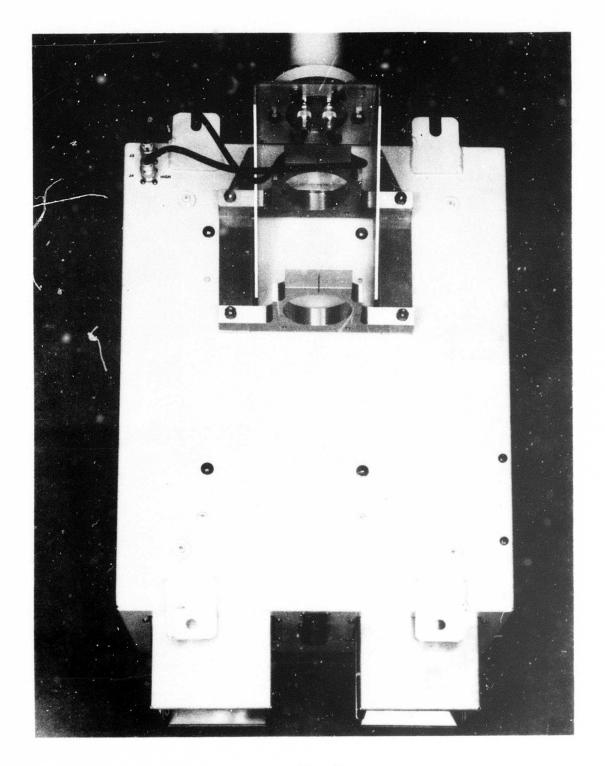
4A-89/4A-90



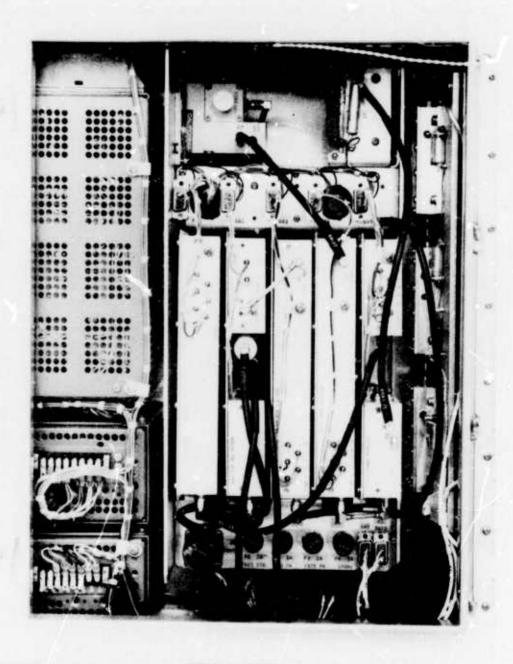




Front View

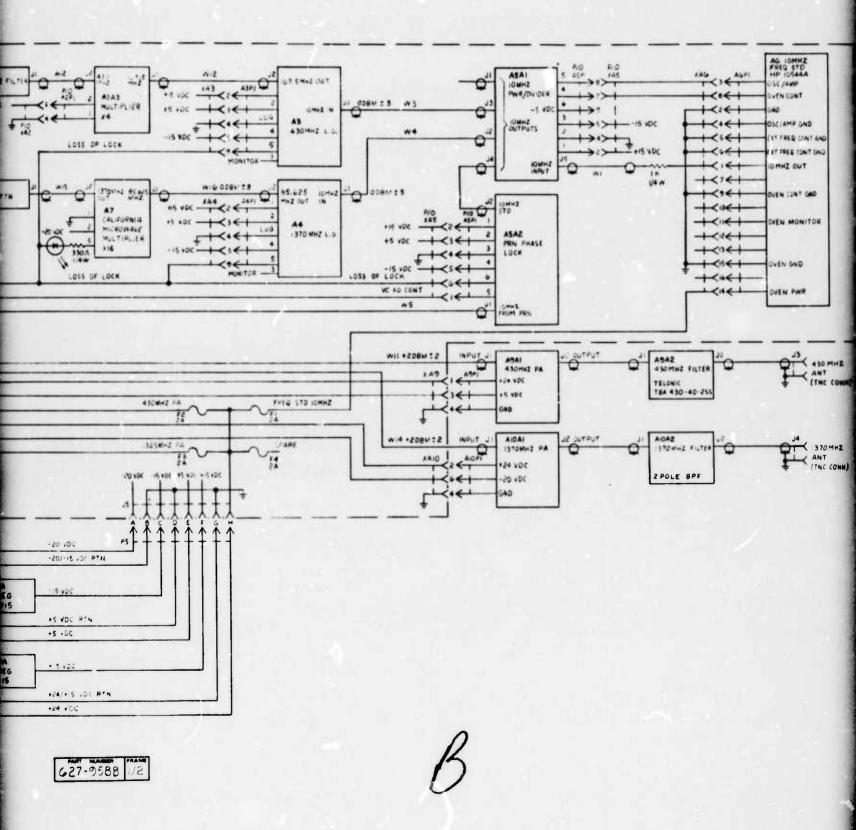


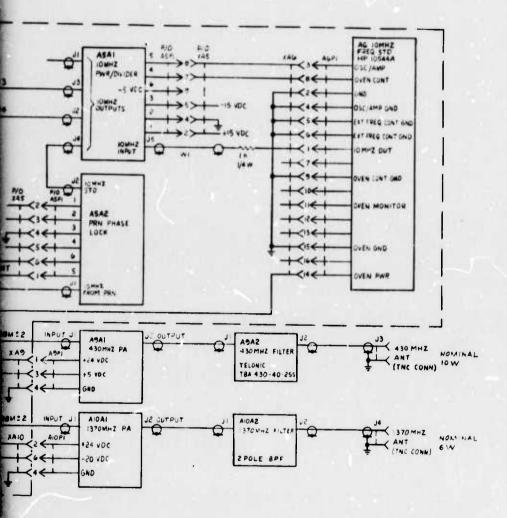
Rear View



Internal

627-9588 1/





REVISIONS

LTB DESCRIPTION DATE APPROVED

-001

REV B CHNG 1325 TO 1370MHZ 3-27-74 REV A FD CHNG 1-25-74

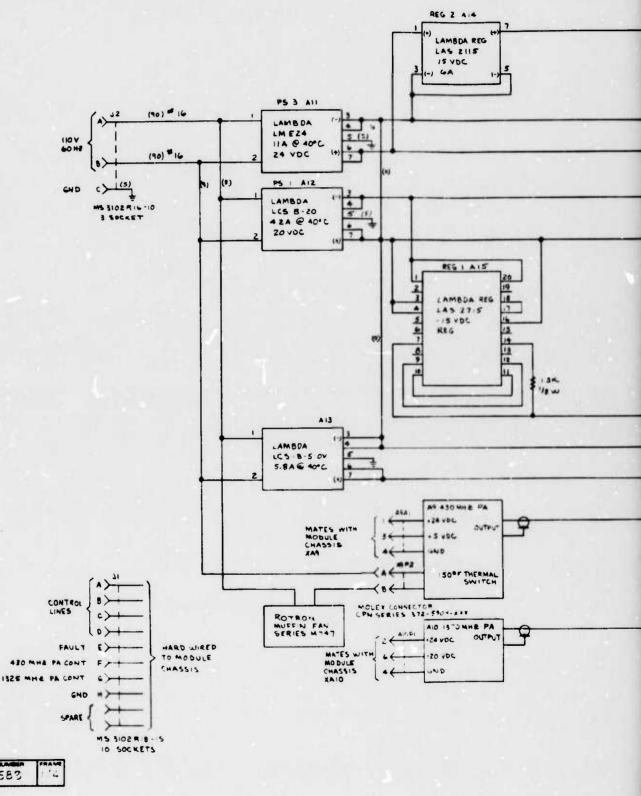
CONTRACT NO.	COLLINS RADIO COMPANY
PREP & W kingled 11 3 13	BLOCK DIAGRAM
СНК	AMTR
APIO .	PACKET RADIO TEST SET
	DH 13499 OWG NO. 627-9588
	SCALE V. VE SHEET

4A-97/4A-98

B

NOTES:

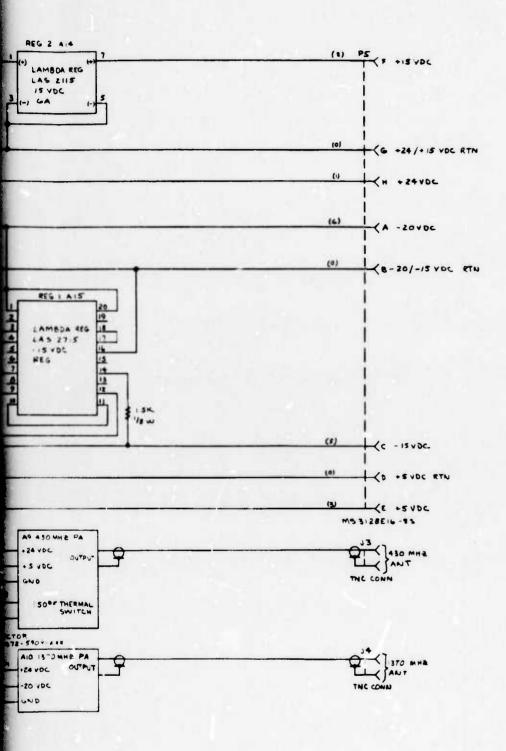
- 1. ALL WIRE #12 TEFLON UNLESS
 OTHERWISE NOTED. COLOR CODE IN ()
- 2, APPI AND APOPI ARE CINCH 9 PIN CONNECTORS
- 3, MS BIOZR SERIES CONNECTORS MATES WITH MS BIOG SERIES PLUGS.



A

627-9583





-001

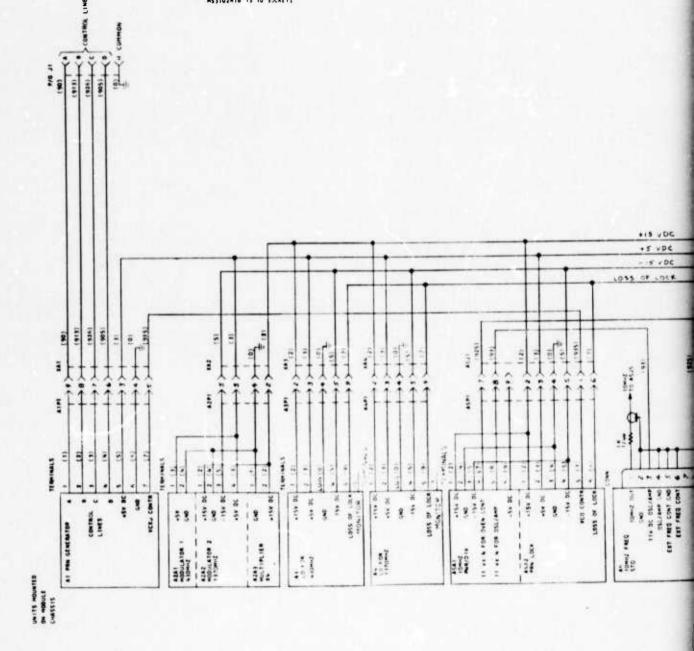
REV A CAMG 1325 TO 137	OMHZ 3-27-74	PUBLICATIONS DRAWING REVISIONS TO BY APPRICATE AND MADE BY "UB ICATIONS ILLUSTRATING DEPARTMENT				
CONTRACT AU	ENCLOSUPE PACKET RAD TEST IMTR					
PREP 1 to shopfed 11 21 73						
CHK						
APVD						
	Dm 1349	9 0WG NO 327-3589				
	SCALE NUNE	SHEET				
		302				





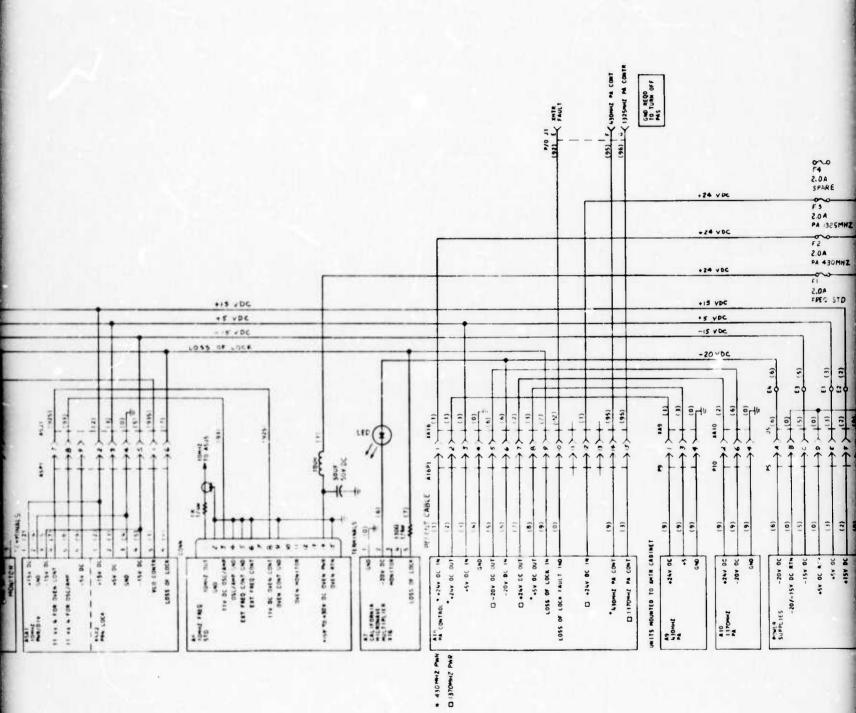
- NOTES

 1. UNLESS OTHERWISE NOTED
 ALL CHASSIS WIPE NO 22
 TEFLON WITH COLOR CODE
 NOTEO IN ()
 2. CONNECTOR JI MOUNTS TO
 UNTA CABINET AND IS AN
 MS3102RIB 15 10 SOCKETS



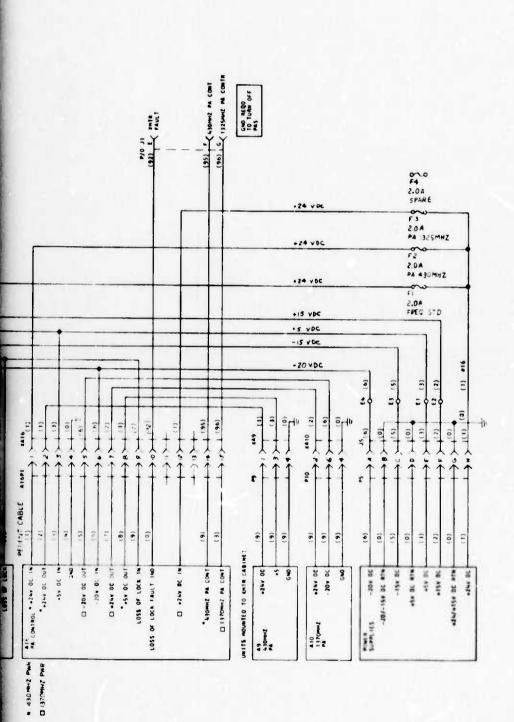
FRAME 627 9550

27-3585



127-3585 5/4

63

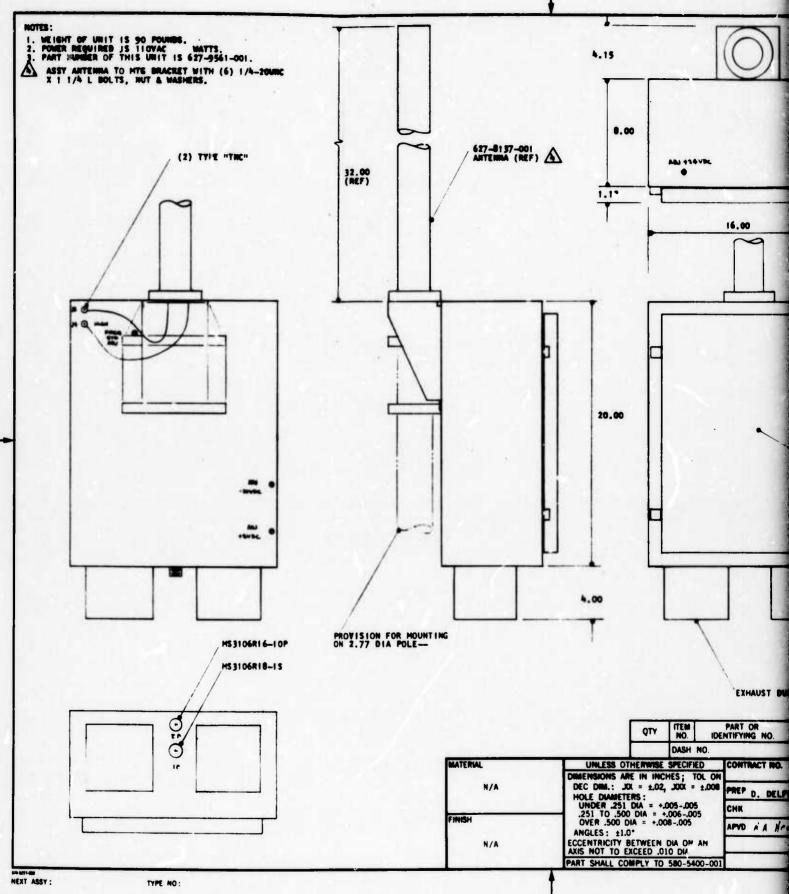


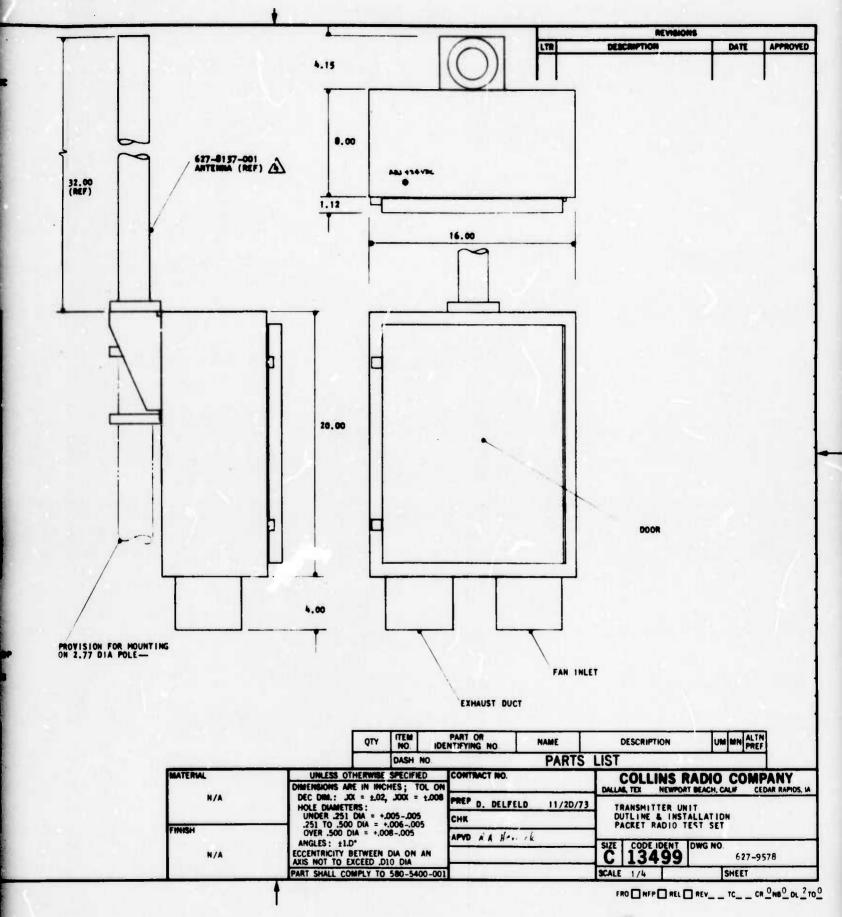
REVISIONS

LTR DESERVETION DATE APPROVED

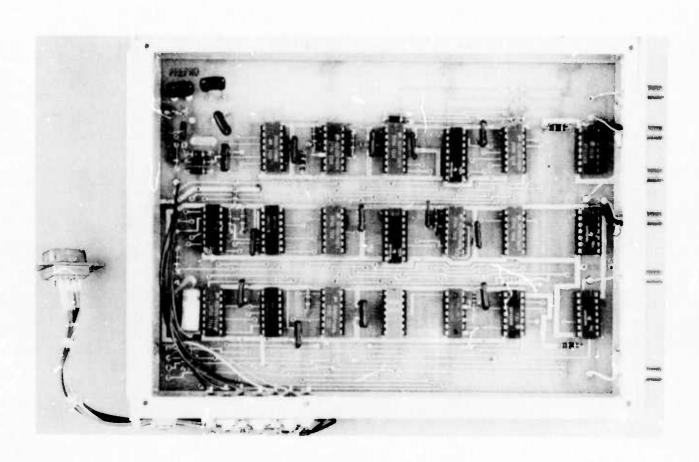
SEV A CHMG 1325 TO 1370MHZ	3-27-74	PUBLICATIONS DRAWING REVISIONS TO BE ARTHURED AND MADE BY 10095 BILLUSTRATING, 144-MINT			
CONTRACT NO	COLLINS RADIO COMPANY				
PREP & W. Khingleil	Was Salaukam				
CHR	MODILE				
APVO	SIZE CODE ID	ENT DWG NO			
	D. 1349	95:3			
	SCALE & VE	SHEET, E			



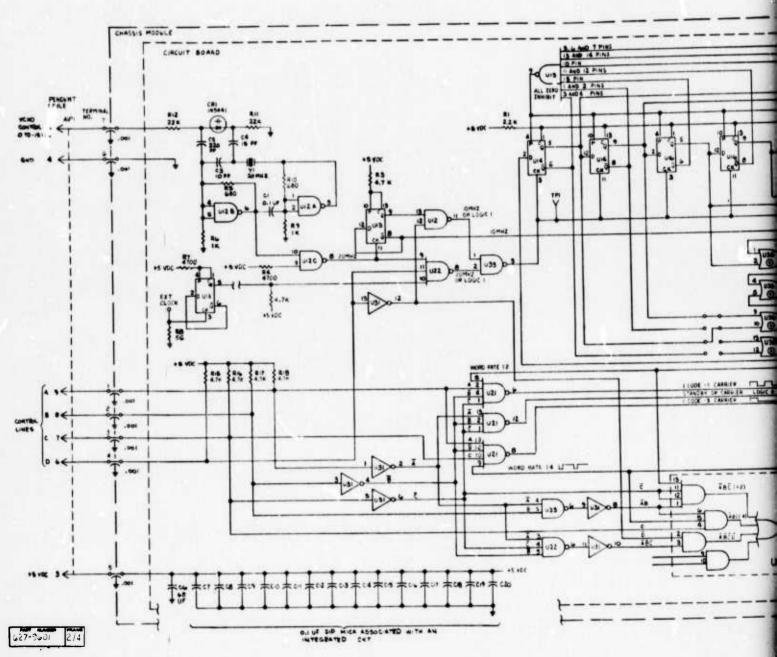


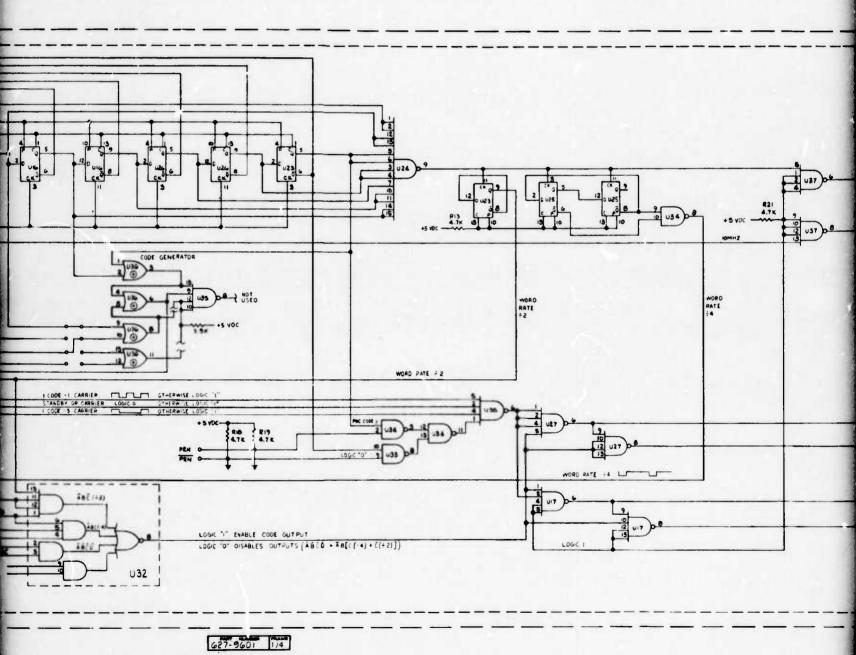




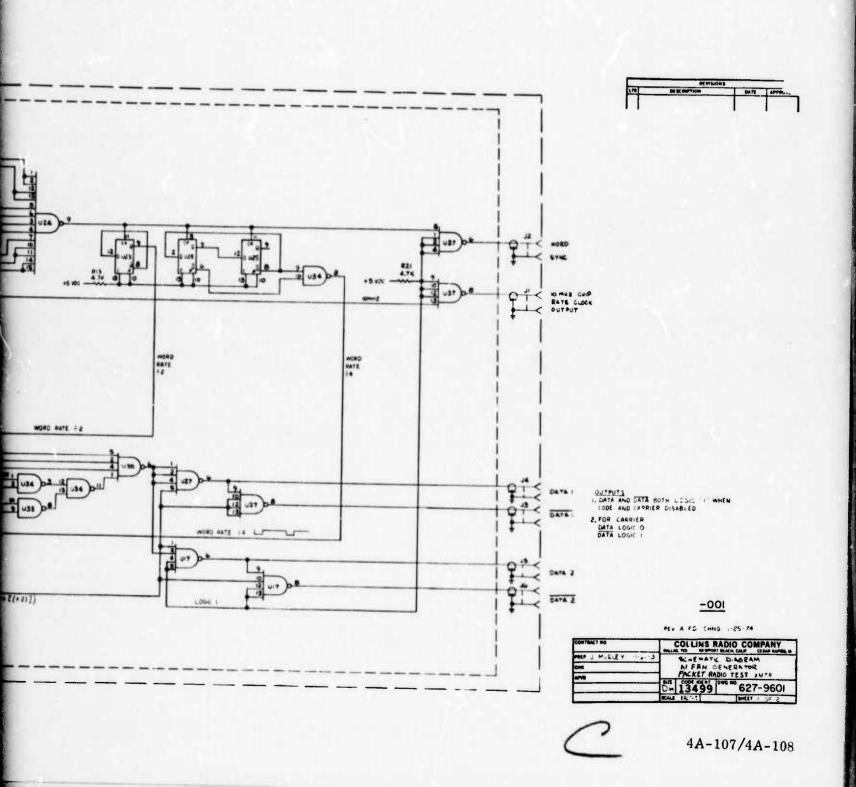


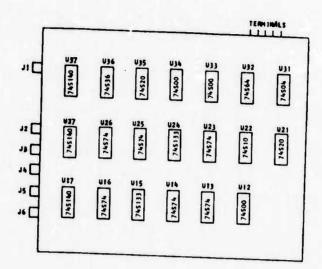
A1 - PRN Code Generator





B

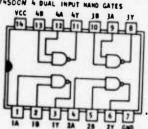




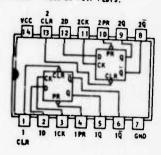
2. CONTROL LINE TRUTH TABLE

CONTROL LINES		INES	******					
A		C	9	OPERATION DESCRIPTION				
0	0	9	0	STANDET				
0	0	0		Cw				
0	0	1	0	CONT CODE AT 10 MCPS				
•	0	1	1	CONT CODE AT 20 MCPS				
	1	0	0	1 0006				
0	1	0	1	1 COOF - 1 CARRIER OF AT TO PEPS				
	1	. 1	0	I COME I CARRIER OFF MI 20 MEPS				
	1	1	1	S CHARLES OFF AT 10 MCPS				
	0	0	0	1 CANS				
		0	1	I cope				
	0	1	0	1 cont				
		1	1	I CODE - 3 CARRIER AT 10 ACPS				

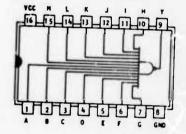
- 1 IS DPEN CKT (BECOMES TTL LOGIC "I")
- O IS GNO (TTL LOGIC "O")
- 3. IC TYPE S (VCC +SV DC) TOP VIEWS
- A. U12/U33/U34 TI SN7450CM & BUAL INPUT NAND GATES



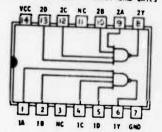
U19/U14/U16/U23/U25/U26 T1 SN 74574M DUAL "9" TYPE POSITIVE EDGE TRIGGERED FLIP FLOPS.



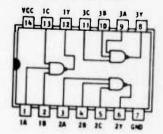
C. UIS/UZ4 TI SN74SI33N I3 INPUT HAND GATE



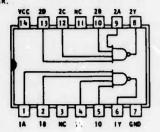
D. U21/U35 T1 SN74S20N DUAL 4 INPUT NAND GATES



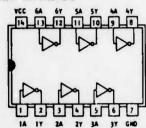
E. UZZ T1 SN74S1DN 3 INPUT NAND GATES



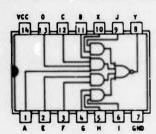
F. U17/U27/U37 TI SN75SIGON QUAL & INPUT NAMD 50 OPPS LINE ORIVER.



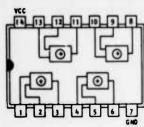
G. U31 TISH74504 HEX INVERTERS



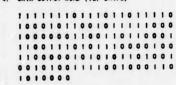
H. U32 TISN74864N 4-2-3-2 INPUT AND OR INVERT GATES

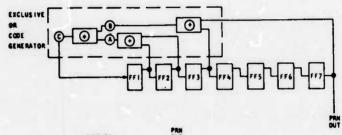


1. U36 NATIONAL SEMICONDUCTOR OM 74586N & QUAL INPUT EXCLUSIVE OR GATES



4. OATA OUTPUT WORD (127 CHIPS)



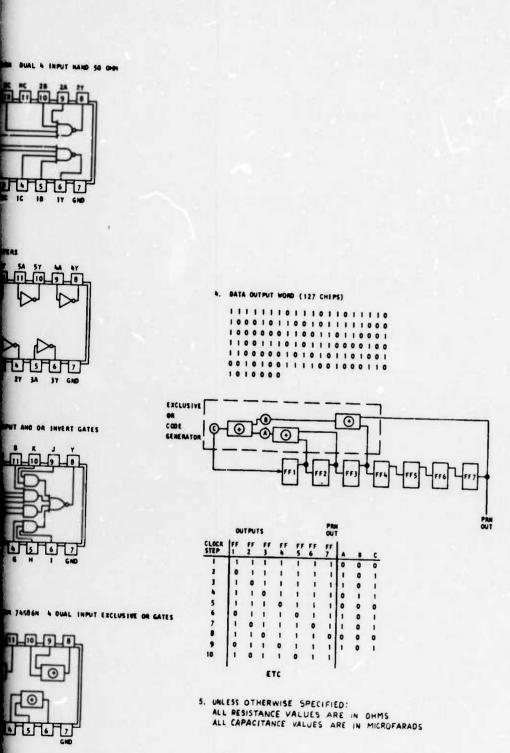


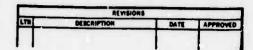
OUTPUTS					TUO					
CLOCK	FF 1	FF 2	FF 3	FF	FF 5	FF 6	FF 7	A		c
1	I	ī	T	1	Ī	1	- 1	0	0	0
2	0	- 1	1	-1	1	- 1	- 1	1	0	- 1
3	1	0	1	- 1	1	- 1	1	1	0	1
4	1	- 1	0	- 1	1	1	- 1	0	1	- 1
5	1	1	1	0	-1	- 1	- 1	0	0	0
6	0	1	1	1	0	- 1	- 1	1	0	- 1
7	1	0	-1	- 1	1	0	1	1	0	- 1
	1	- 1	0	- 1	1	- 1	0	0	0	0
9	0	- 1	1	0	1	- 1	- 1	1	0	1
10	1	0	1	1	0	- 1	1			
	•			TC				•		

5. UNLESS OTHERWISE SPECIFIED:
ALL RESISTANCE VALUES ARE IN OHMS
ALL CAPACITANCE VALUES ARE IN MICROFARADS

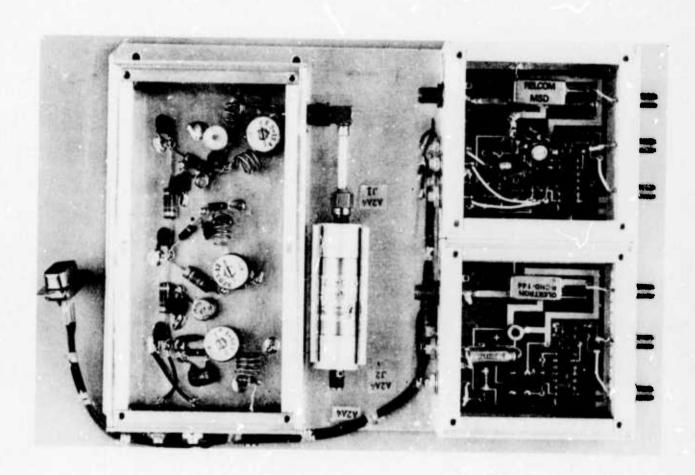


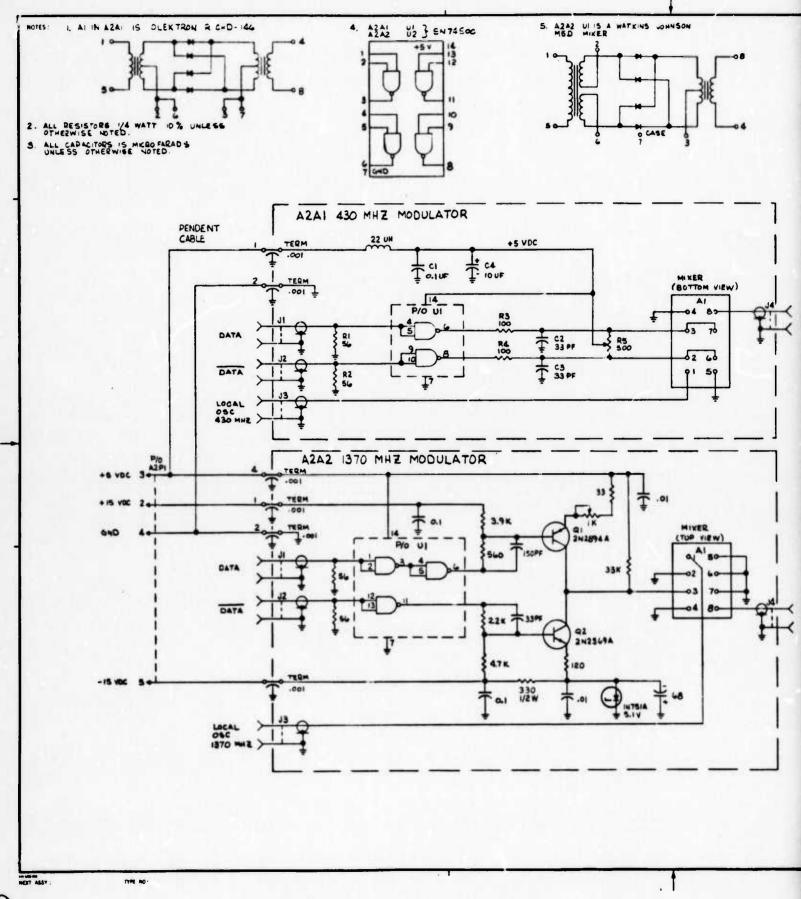




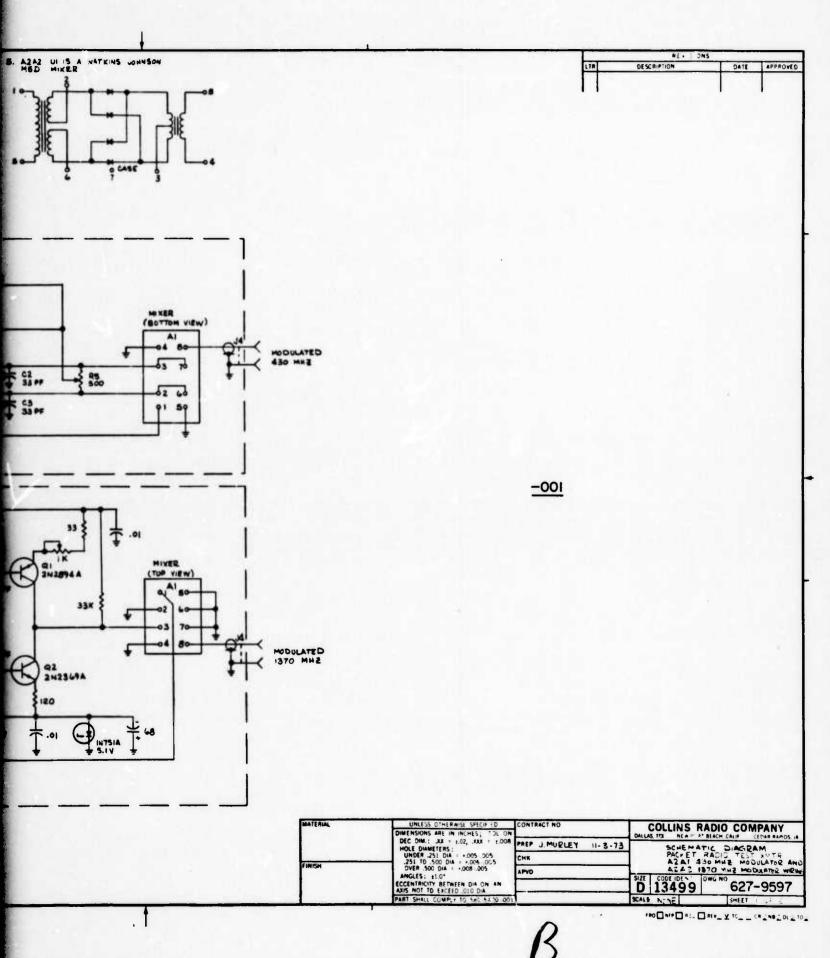


C

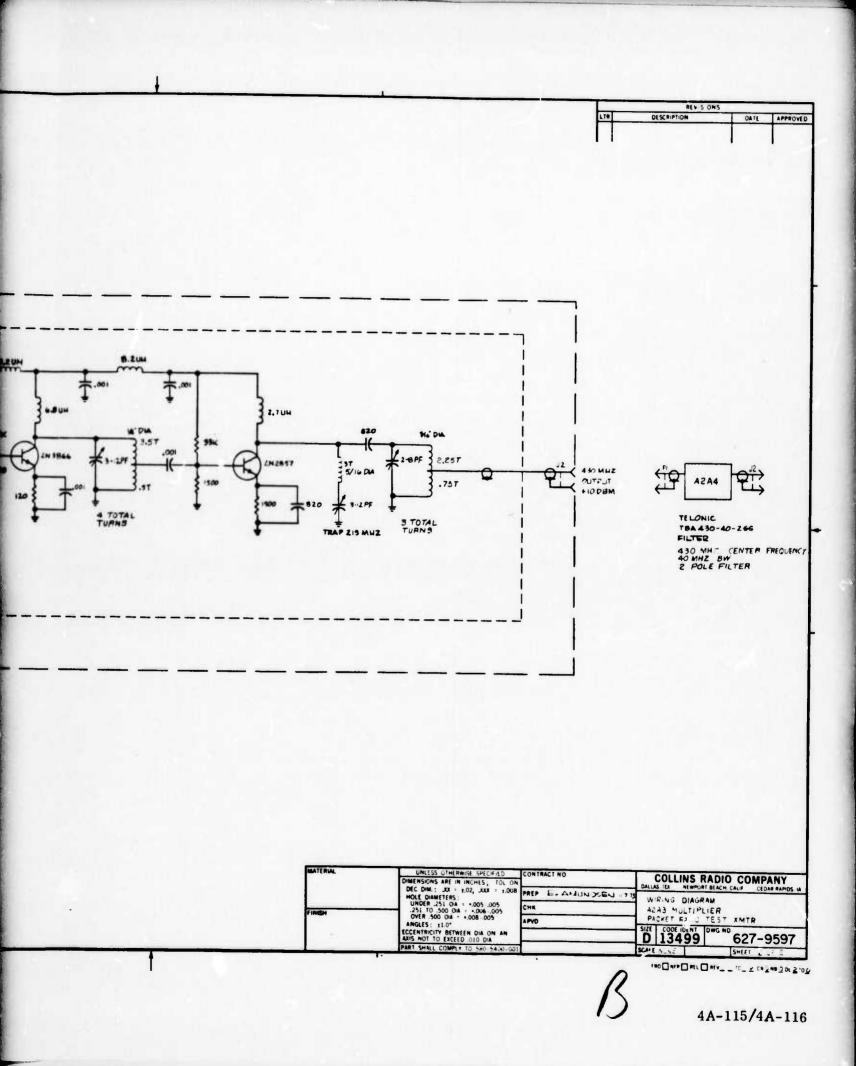


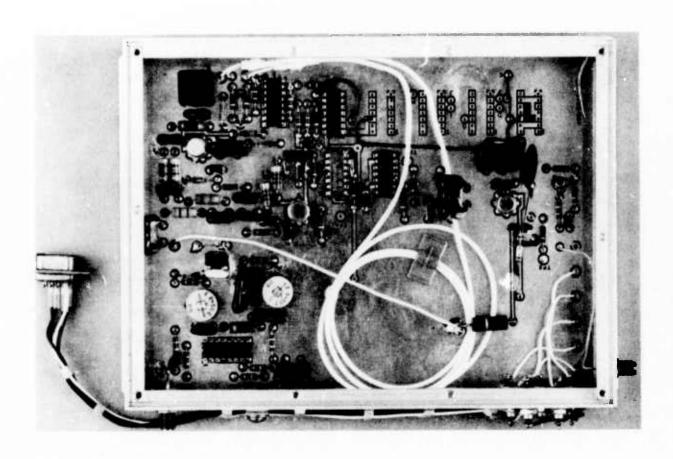


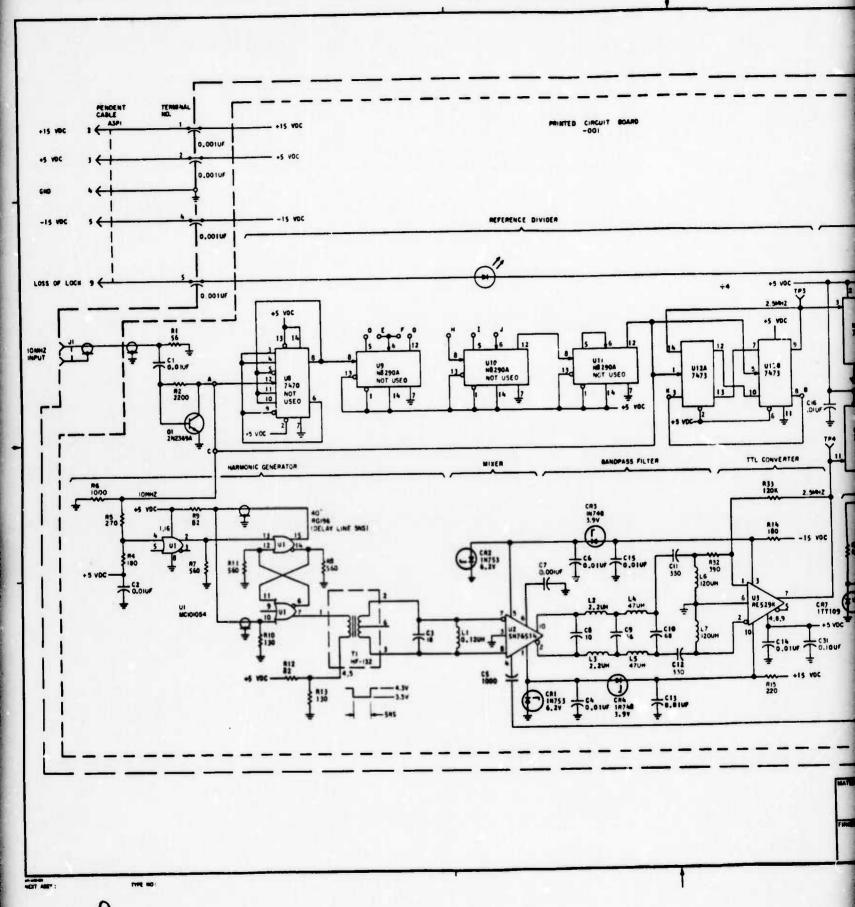
P

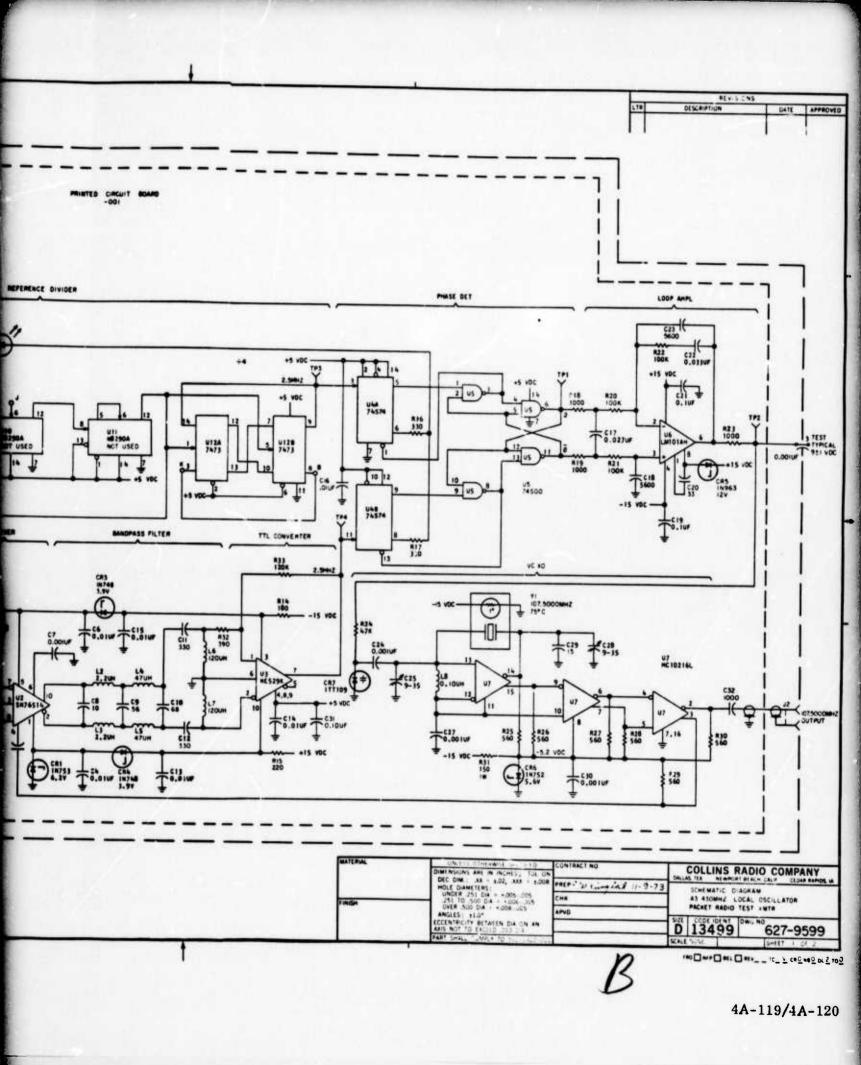


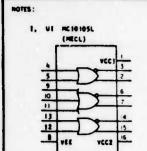
HOTES: I. UNLESS OTHERWISE SPECIFIED, ALL CAPACITOR VALUES ARE IN MICROFARADS ALL RESISTANCE VALUES ARE IN OHMS 2. COILS MADE FROM NO ZO BUSS WIRE EASA PENDENT P/O AZPI TERM +15 VDC 2 4 ,001 TO OTHER MODULES IO7.500MHZ 5 TOTAL 4 TOTAL

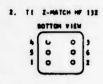




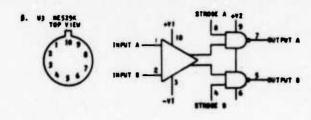


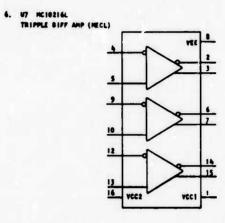


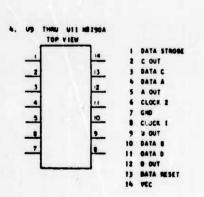




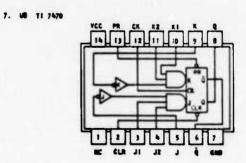








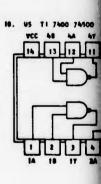
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8. WIZ TI 7473

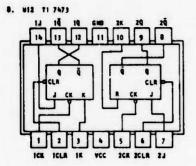
14 14



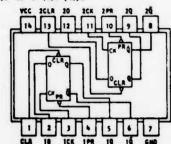
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LTR DESCRIPTION DATE APPROVED

BUTPUT A

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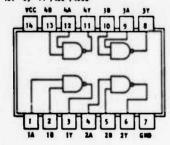


9. W TI 7674 74574



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ALL RESISTANCE VALUES ARE IN OHMS
ALL RESISTORS ARE 1/4 W CARBON
ALL CAPACITANCE VALUES ARE IN PICOFARADS.

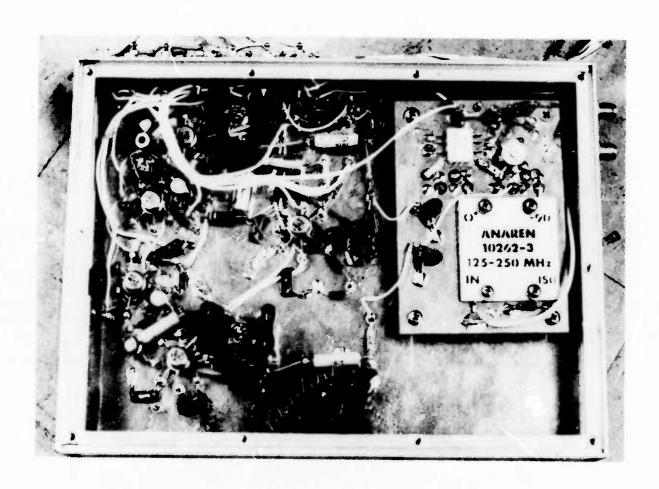
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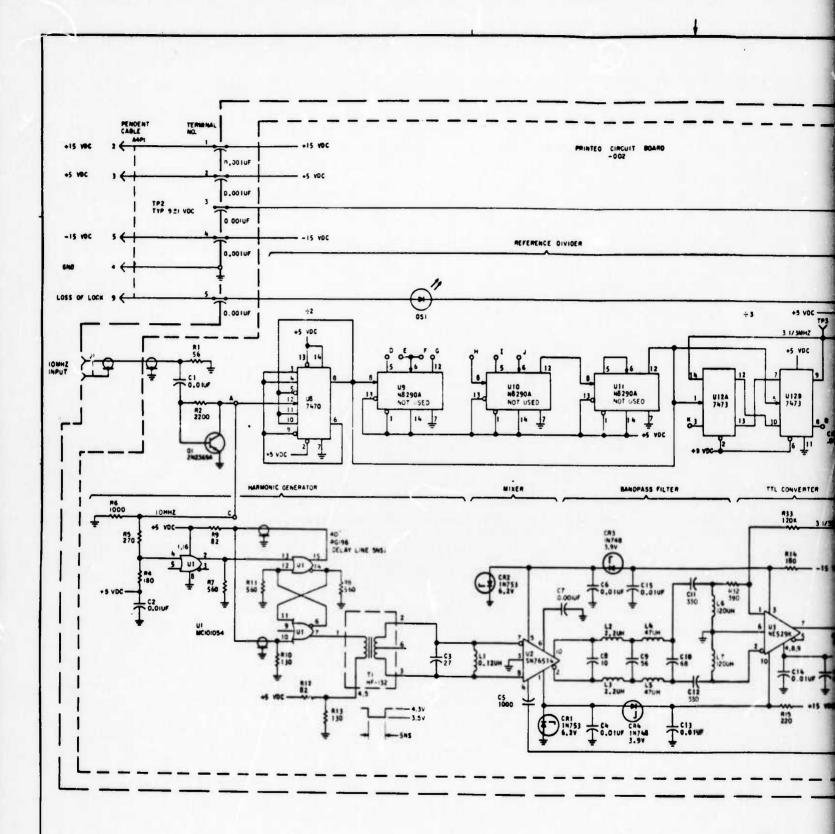


D 13499 0627-9599

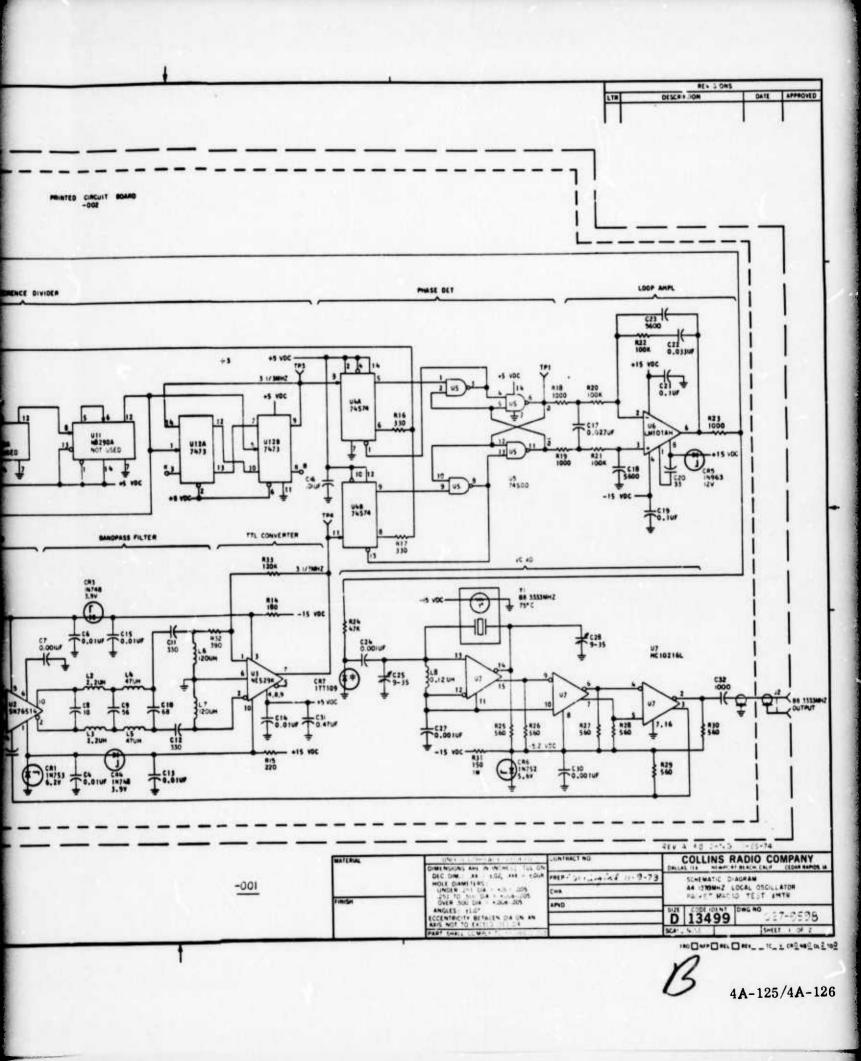
| Sept. | None | Per | Sheet | 2 of 2





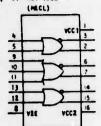


-001





1, U1 MC1010SL



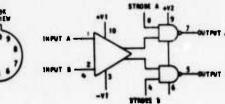
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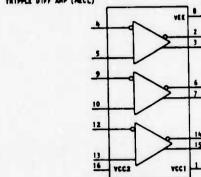
3. W2 SH76514 TOP VIEW



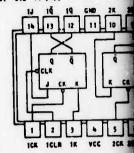
S. US NESZSK TOP VIEW



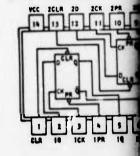
6. UT HCIDZIGL TRIPPLE DIFF AMP (MECL)



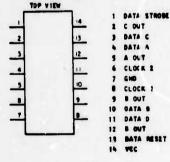
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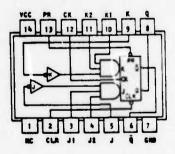
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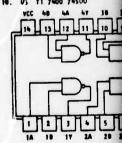
UP THRU U11 HB290A TDP V1EW



7. US T1 7470



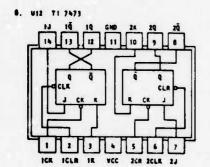
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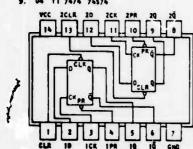
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OUTPUT A

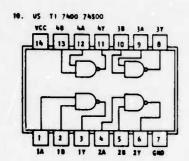
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9. US TI 7474 74574

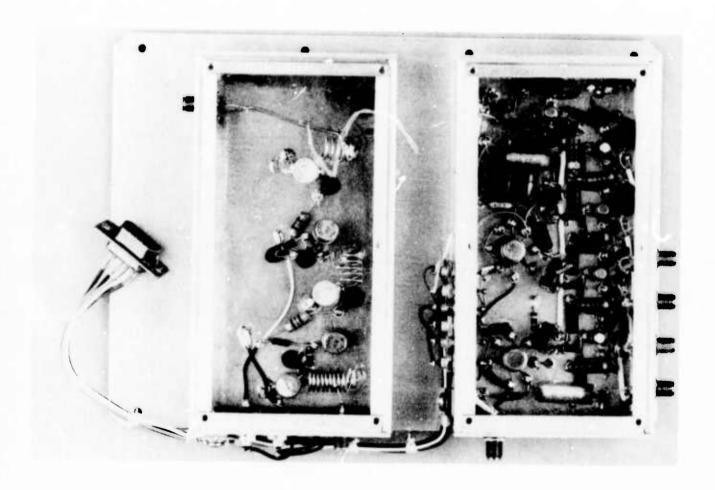


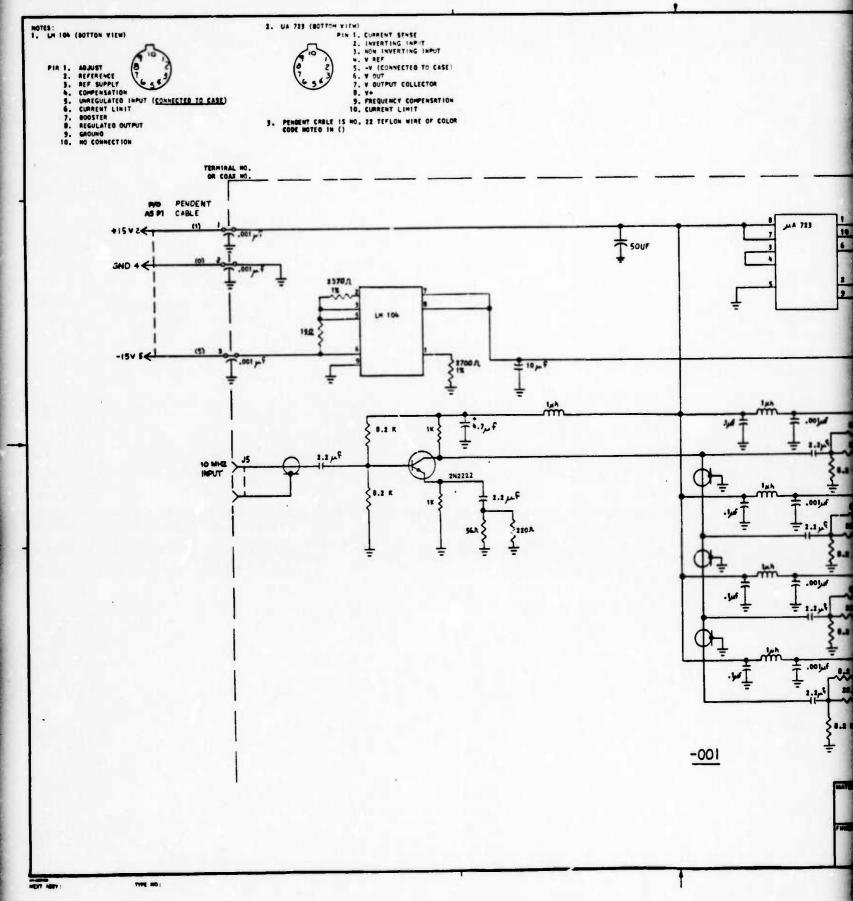
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ALL RESISTORS ARE 1/4 W CARBON
ALL CAPACITANCE VALUES ARE IN PICOFARADB.

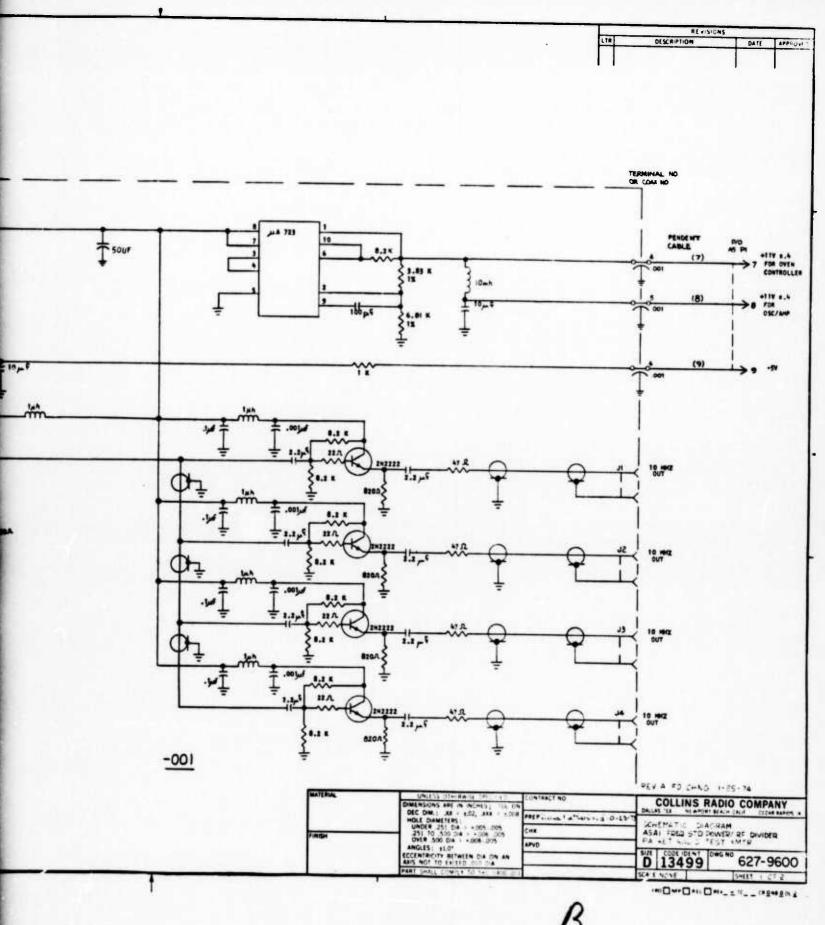


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| SALE NONE | PEV | SMEET 2 OF 2

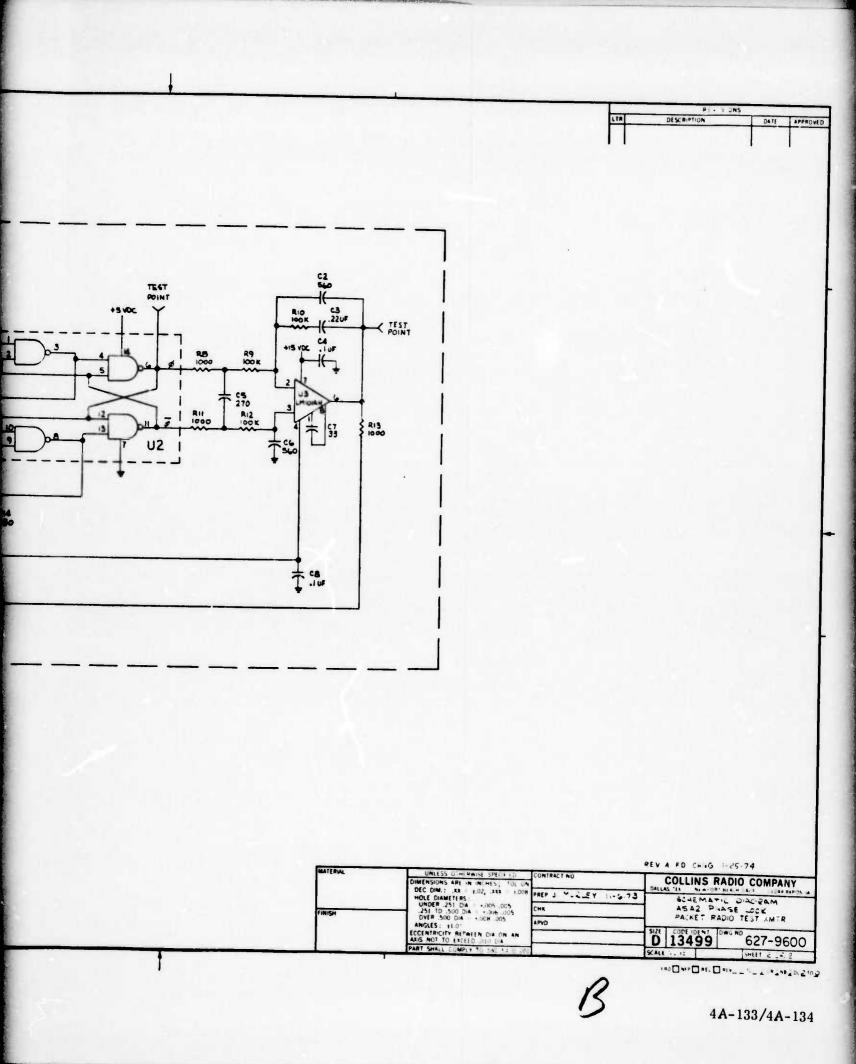


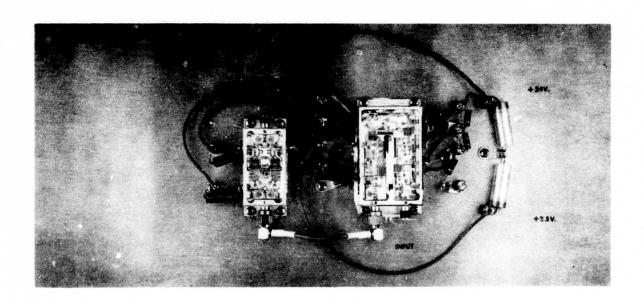


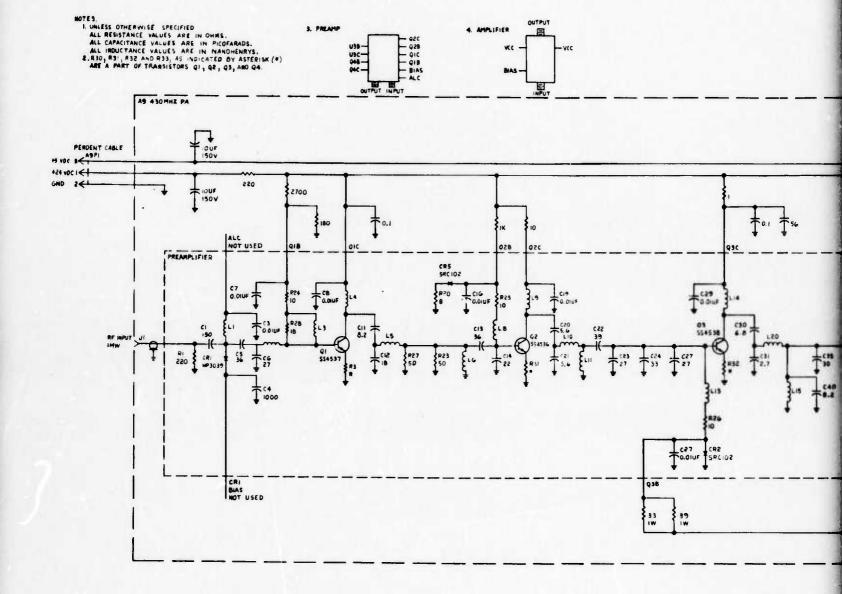


4A-131/4A-132

MOTES: 1. ALL RESISTORS 14 W 10% UNLESS STHERWISE NOTED.
2. ALL CAPACITORS IN PICOFARADS UNLESS STHERWISE NOTED.
3. UZ 15 74500
4. UI 15 74573 SAZA PENDENT CABLE TERMINAL NO. +15 VOC 2 C1 .010F .001 U2 815 R14 330 330 -301 UF . 001 UF (1) 5 VOLTAGE . 001 UF MENT ASSY: IVE O.





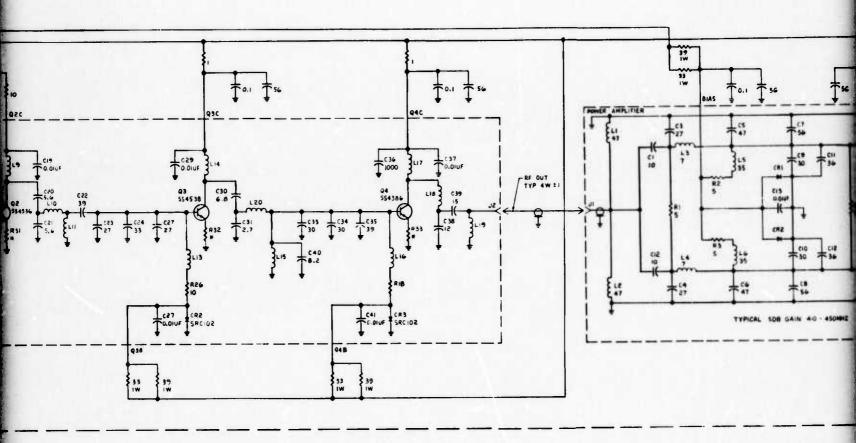


627-9651 3/3

627-9651 2/3

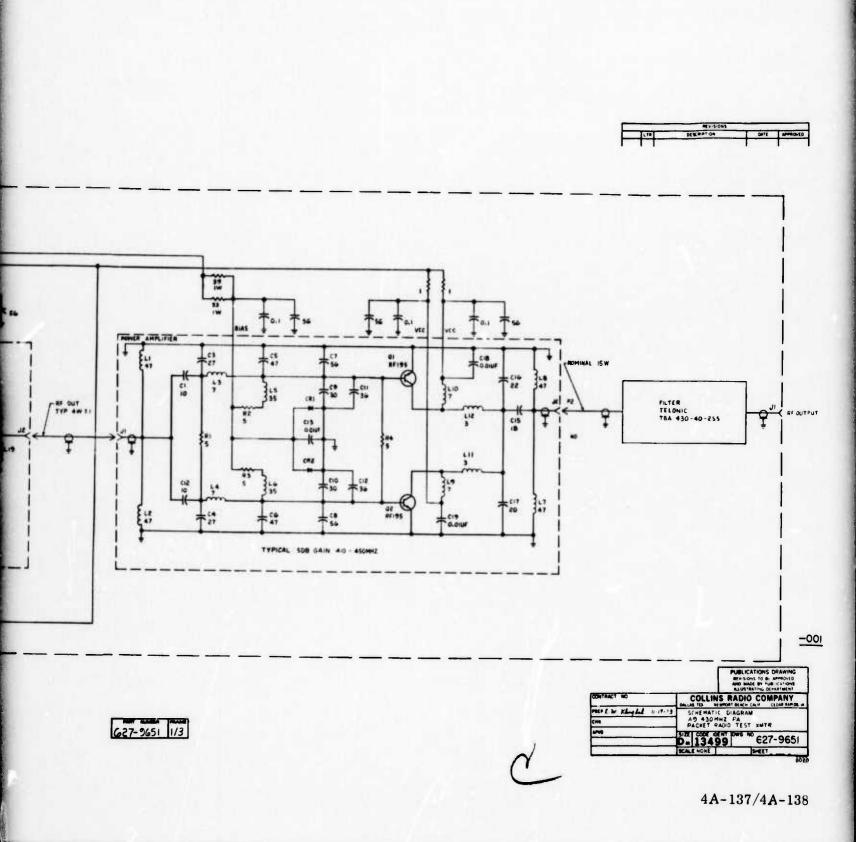
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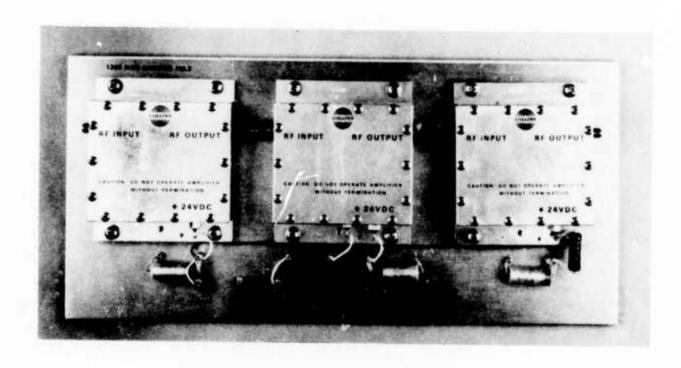




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627-9651 1/3



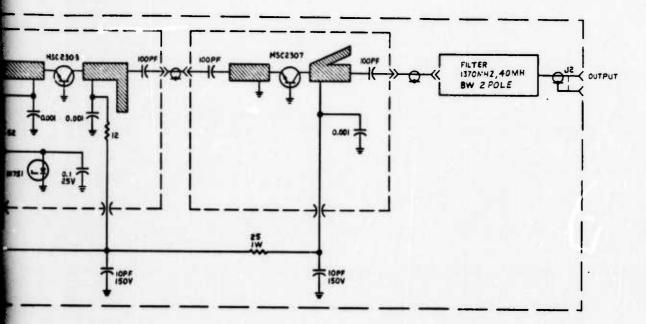


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LTR DESCRIPTION DATE APPROVED



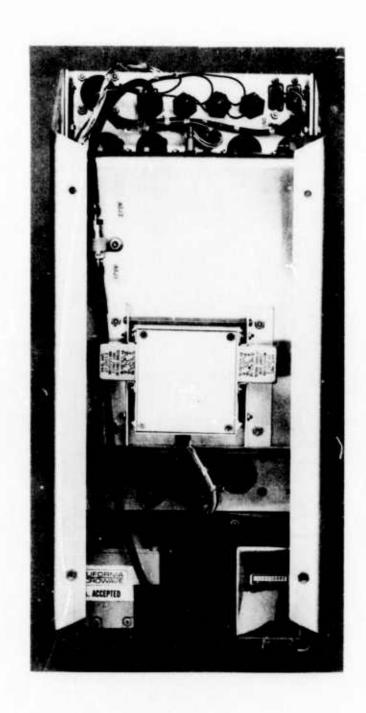
-001

DIMENSIONS ARE IN INCHES; TOL ON DEC DIM.: JX = 1.02, JXX = 1.008 MDLE DIMERERS: UNDER .251 ID = 4.005 .005 UNDER .251 ID = 4.006 .005 OVER .500 DIA = 4.006 .005 ANGLES: ±1.0° ECCENTRICITY BETWEEN DIA DIN AN AXIS NOT TO EXCESO .010 DIA AND AXIS NOT TO EXCESO .010 DIA AX

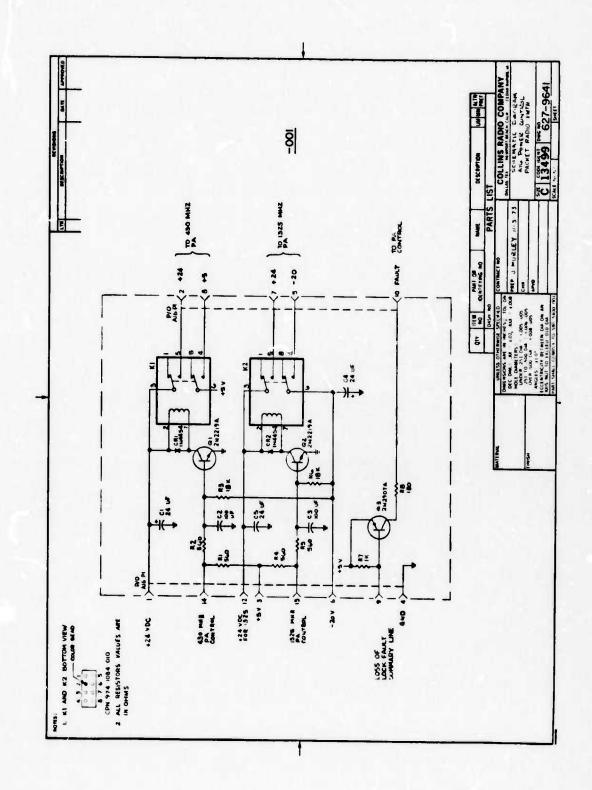
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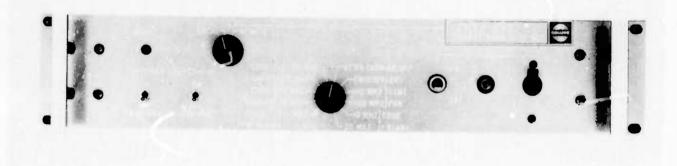
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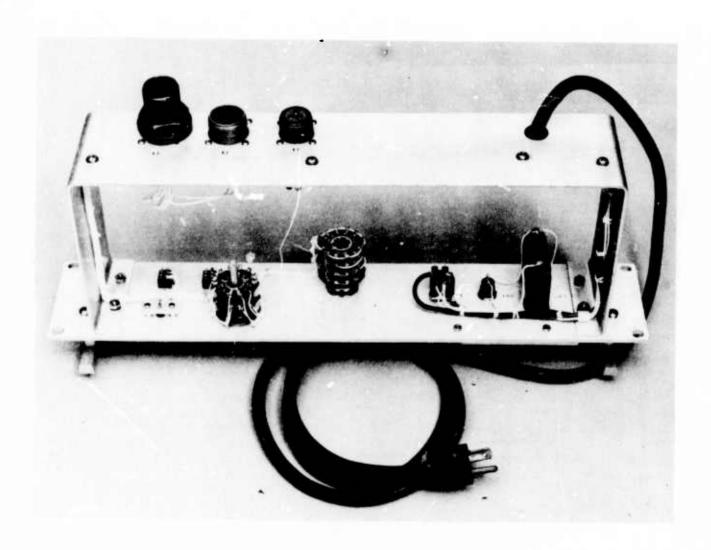
4A-141/4A-142



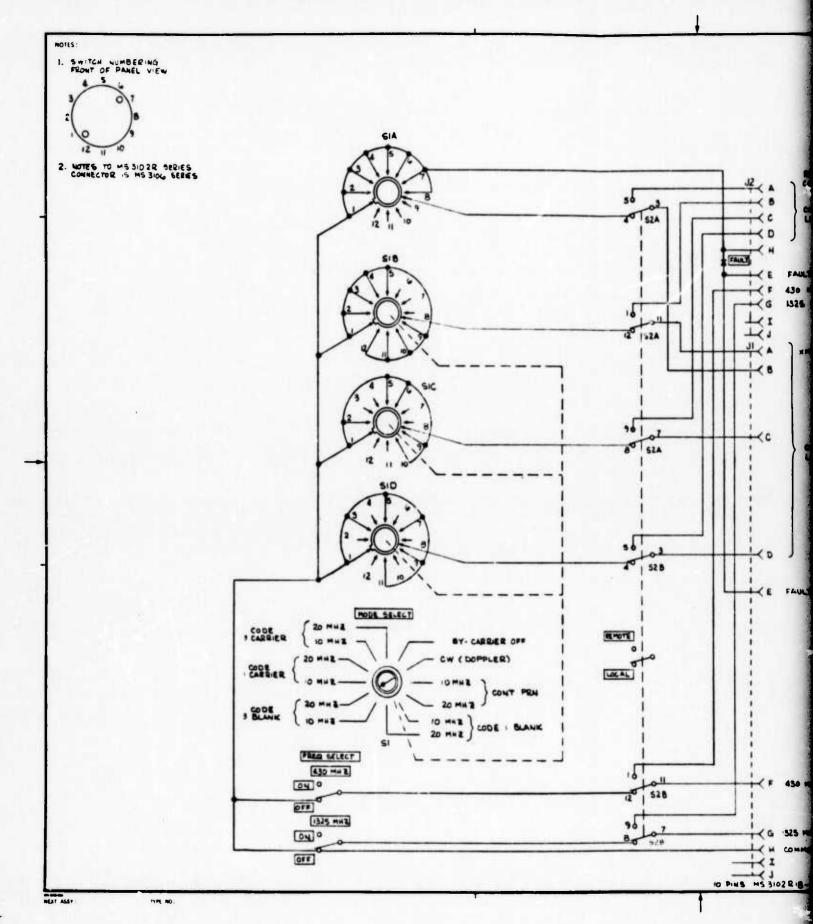
A16 - POWER CONTROL



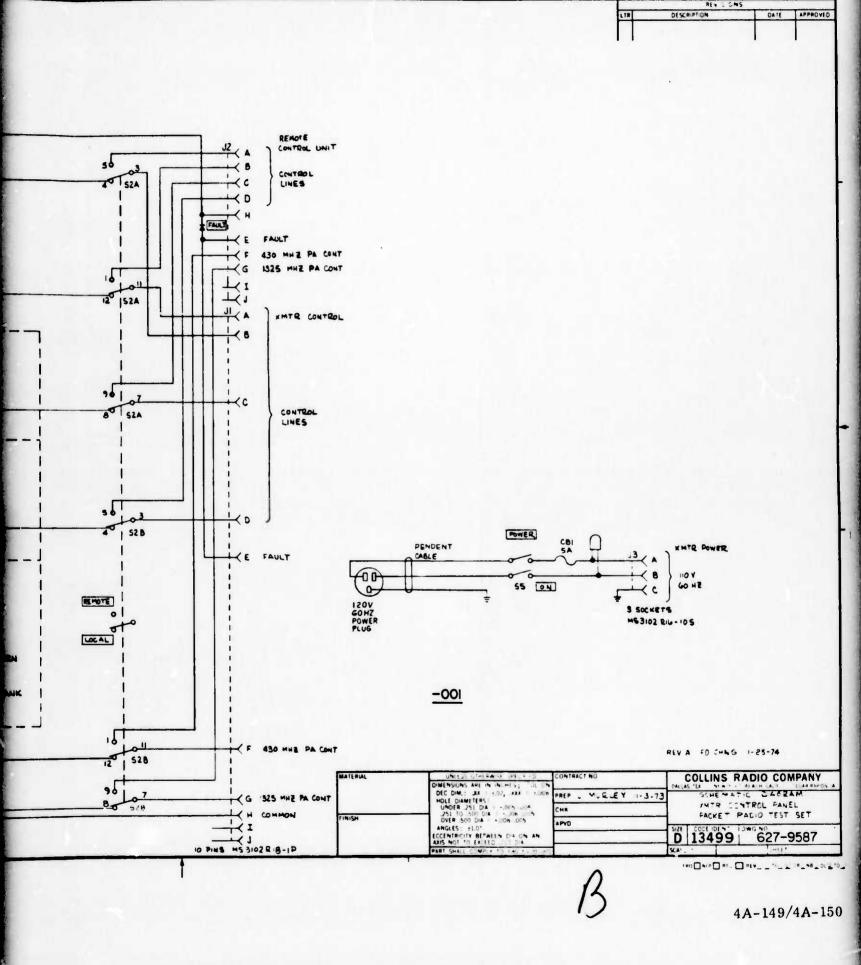


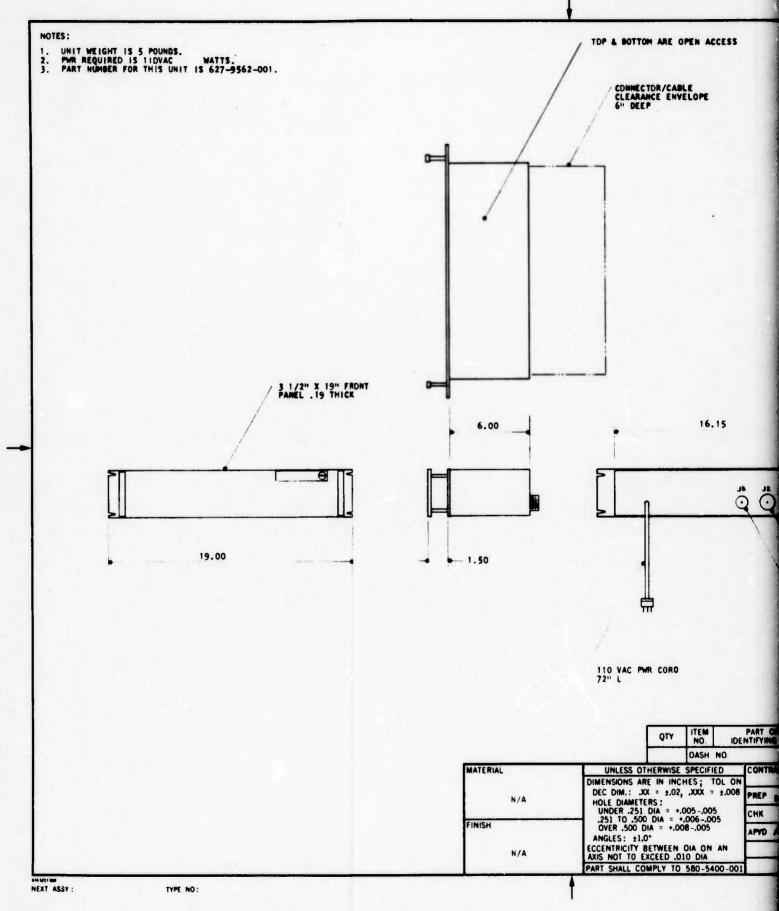


Assembly

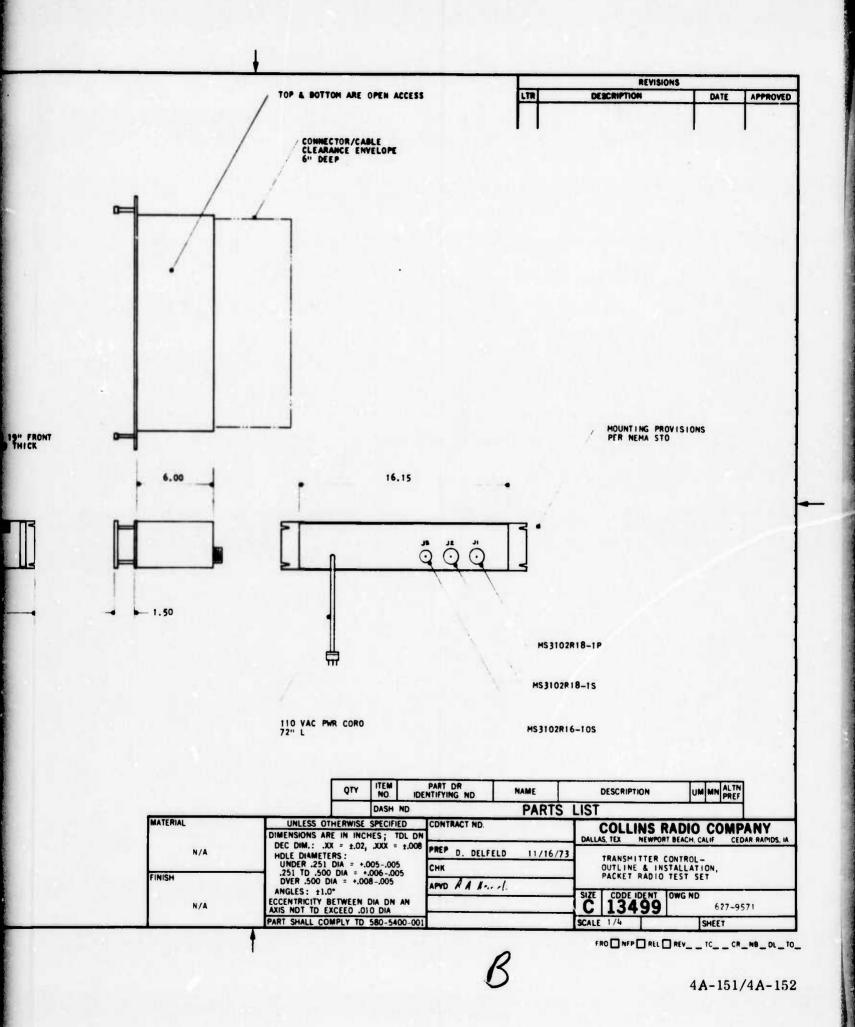


A



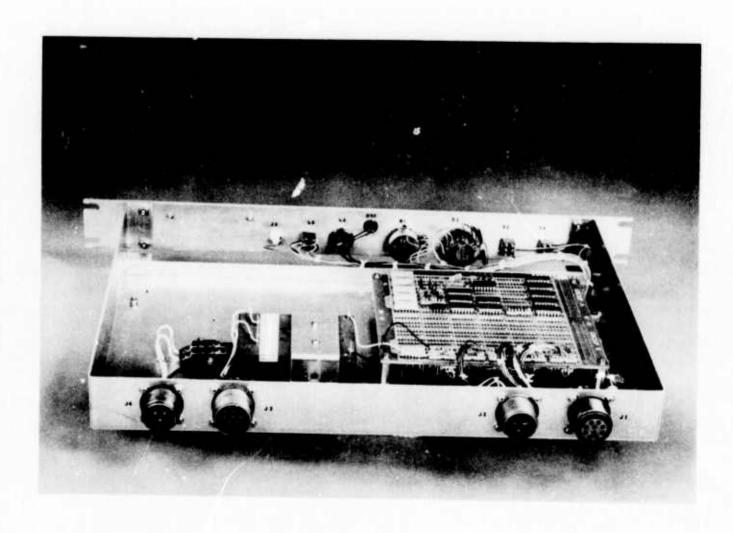


A





Front Panel

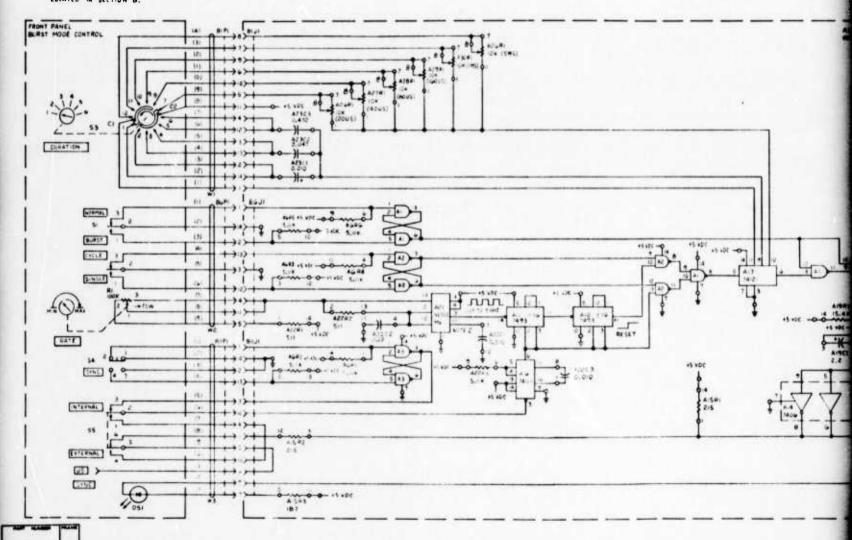


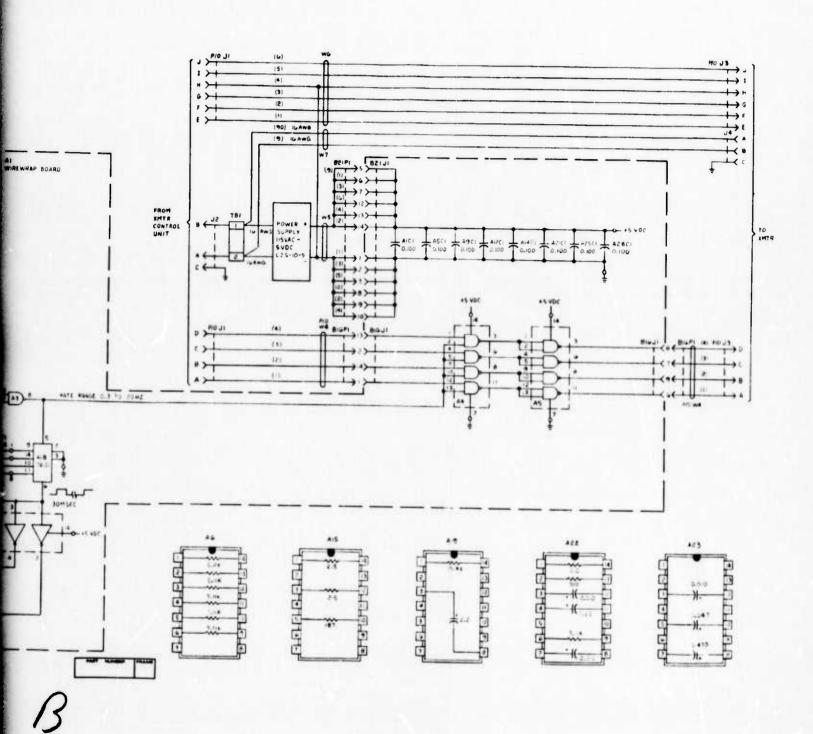
Assembly

NOTES:

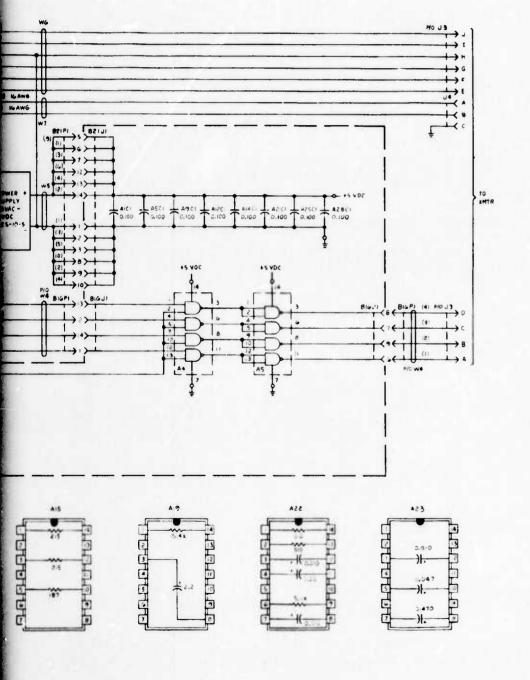
1. UNLESS CHERWISE SPECIFIED
ALL RESSISTANCE VALUES ARE IN OHMS
ALL CARACITANCE VALUES ARE IN MICROFARADS
ALL WIRE BYZ TEFLON, WITH COLOR CODE IN ()
2. THE 555 TIMER IS MOUNTED AT POSITION AZI
WITH PIN1 OF THE COMPONENTS MATING WITH
PIN1 OF THE BOARD.
3. ALL AUDIO CONNECTIONS FROM BOARD AT ARE
LOCATED IN SECTION B.

4 CIRCUIT CARD GND FLOATING WITH RESPECT TO CHASSIS GND.

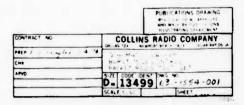




PRIP / . . CHR

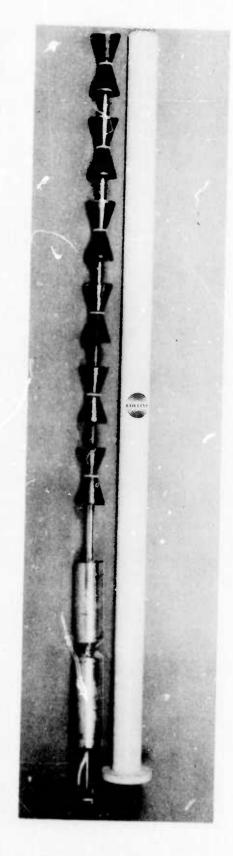




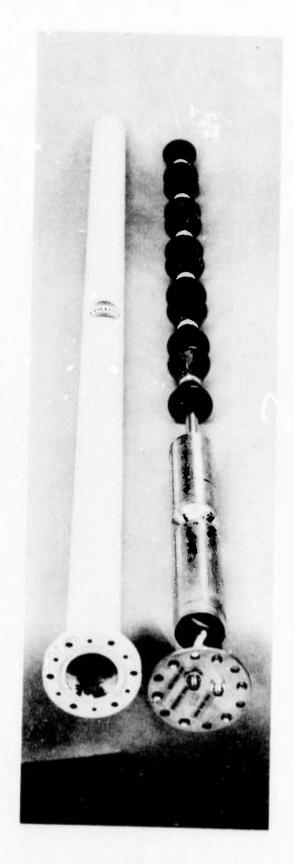




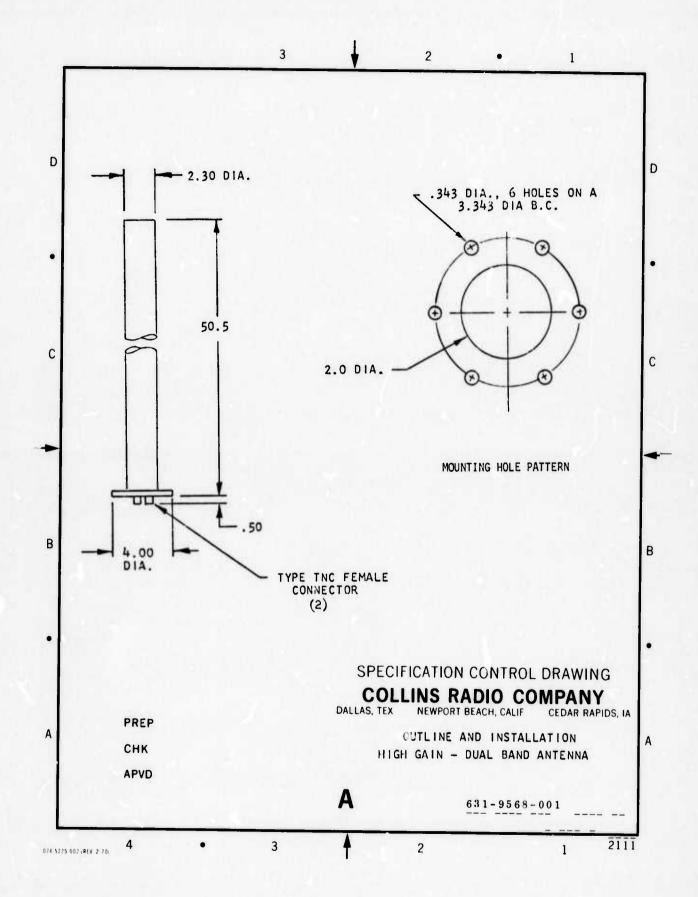
4A-155/4A-156



Assembly View



Assembly View



B.1 INTRODUCTION

Although the test set has been designed to allow the user to adjust many levels for specific tests, two alignment procedures are suggested.

- a. IF channel gain and receiver signal meter calibration
- b. Doppler test setup

The if. channel gain adjustments normalize all signals (430 MHz RCV, 1370 MHz RCV, wideband or narrowband) to a constant level for monitoring or processing.

The front panel receive signal strength meter operates on the agc voltage and is only usable when in the automatic agc mode. It provides a gross signal strength indication to the operator.

Doppler tests may be made in open loop or phase-lock mode. The frequency standards in the receiver and transmitter have sufficiently low drift rate to allow short period measurements, provided the oscillators are carefully adjusted for synchronism. A very long loop time constant (minutes) is employed to avoid tracking the low rate doppler expected in tests in an urban environment.

The adjustment procedures reference 1325 MHz which is engraved on the front panel. The test set has been converted to 1370 MHz and the procedures are still valid.

- B.2 ADJUSTMENT PROCEDURE OF IF CHANNEL GAIN AND RCVR SIG METER CALIBRATION
- a. Terminate (50 ohms) both antenna input ports.
- b. Set both if. channel gain controls for max gain (full CW)
- c. Select

Channel 430 MHz

BW WB

IF age Auto

Threshold Det IF

Doppler Test Disable

- d. Adjust automatic age gain level for desired output (put on top of A1)
- e. Adjust the offset control (top of A1 out house) for a reading of 0.2 mA on the RCVR SIG meter.

alignment

- f. Select the 1325 channel. Note the RCVR SIG meter reading.
- g. Adjust the channel with the highest MA reading on the RCVR SIG meter to be equal to the other channel.
- h. Select the NB mode and adjust the NB gain control (located toward the front of module A3A1) for a RCVR SIG meter reading equal to that obtained in step g.
- i. Readjust the offset control on the top of A1 for a reading of 0 mA on the RCVR SIG meter.
- j. Recheck the balance of the NB/WB/430/1325 switch positions.
- k. Apply a 430 or 1325 MHz CW signal at -30 dBm to the appropriate antenna port.
- 1. Adjust the RCVR SIG meter drive control (located on a bracket behind the meter) for a reading of 1.0 mA.
- m. Reterminate the antenna port and readjust the offset control for 0 mA (if required).
- n. Repeat steps j., k., and l. until steps k. and l. are correct without readjustment.
- o. Generate a meter calibration curve.

B.3 DOPPLER TEST SETUP

The phase lock loop to synchronize the receiver to the transmitter is designed to have a very long time constant so that it will not track the doppler shifts at the low doppler rates expected during the tests. The frequency standard also has sufficient stability to allow short-period doppler measurements to be made open loop, provided the frequency is precisely adjusted just prior to the test. Adjustment of the receiver frequency standard to proper phase lock condition is somewhat tedious due to the long time constant. The following procedure is recommended to reduce the time required for this adjustment.

- a. Adjustments for transmitter mode and receiver modes follow:
 - 1. Transmitter Mode CW
 - 2. Receiver Modes

Channel Select 430 MHz or 1325 MHz

BW NB

Doppler Test Disable

IF AGC AMPL Auto

Adjustment Set 10 MHz FREQ CTL for zero beat frequency as

observed on the I&Q meters. This frequency control does not have the doppler time constant delays and zero beat can be obtained in a short period of trial & error adjustment. The I meter should be at zero and the Q meter at -5 volts. The frequency

standard correction voltage can be recorded (to the nearest millivolt) from the front panel test point located below the I&Q meters to minimize alignment in the doppler test mode.

b. If doppler tests are to be made with the receiver locked to the transmitter through the slow loop, proceed to adjust the system as follows:

In the doppler test mode, use the same receiver switch modes as step a. except the doppler test is "ON". Place the \emptyset LL switch to fast. (The loop time constant is still relatively slow in the fast position.) Adjust the 10 MHz \emptyset CTL until the frequency standard correction voltage is the same as that determined in step a.

Allow 30 seconds or more for the doppler test unit to settle to the vicinity of null. Fine adjust the phase control for the I meter to be 0 and the Q meter to be -5V.

Set the $\emptyset LL\ T_c$ switch to slow and slowly readjust the phase control for the proper I&Q meter readings if necessary.

Note: If in the field with doppler affects being displayed, the I&Q meters will never stabilize at the 0 volts and -5-volt positions.

C.1 INTRODUCTION

The data in this appendix is presented without narrative and is considered self-explanatory. The index defines the order of presentation for quick reference. Note that the data reflects the performance at 1325 MHz and was not repeated at 1370 MHz. The performance at 1370 MHz is the same as the data presented for 1325 MHz.

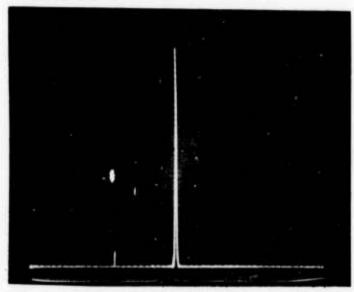
a.	Transmitter RF Spectrums	Page
	1325 MHz	
	CW	4C-3
	Standby	4C-3
	10 M-chip code	4C-4
	20 M-chip code	4C-4
	10 M-chip, 1 code - 1 carrier	4C-5
	20 M-chip, 1 code - 1 carrier	4C-5
	430 MHz	
	CW	4C-6
	Standby	4C-6
	10 M-chip code	4C-7
	20 M-chip code	4C-7
	10 M-chip code, 1 code — 1 carrier	4C-8
	20 M-chip, 1 code — 1 carrier	4C-8
b.	Received Signal as Function of Time	
	10 M-Chip rate	4C-9
	Continuous code	4C-9
	Code — 1 blank	4C-10
	Code — 1 carrier	4C-10
	Code — 3 blank	4C-11
	Code — 3 carrier	4C-11

performance data

	20 M-Chip rate	Page 4C-12
		40-12
	Continuous code	4C-12
	Code — 1 blank	4C-13
	Code — 1 carrier	4C-13
	Code — 3 blank	4C-14
	Code — 3 carrier	4C-14
c.	SAWD Interactions	
	10 M-Chip Xmt - 20 M-chip RCV	4C-15
	20 M-Chip Xmt - 10 M-chip RCV	4C-15
d.	Miscellaneous Radio Data	
	Envelope Det Response	4C-17
	Threshold Detector Impulse Response	4C-17
e.	Antenna Patterns	
	Low Gain Ant	
	430 MHz (2 dBI)	
	Azimuth Plane w/o gnd plane	4C-19
	Elevation Plane w/o gnd plane	4C-20
	Elevation Plane with gnd plane	4C-21
	1325 MHz (2 dBI)	
	Azimuth Plane w/o gnd plane	4C-22
	Elevation Plane w/o gnd plane	4C-23
	Elevation Plane with gnd plane	4C-24
	1370 MHz	
	Elevation Plane w/o gnd plane	4C-25
	High Gain Antenna	
	430 MHz (2 dBi)	
	Elevation Plane w/o gnd plane	4C-26
	1370 MHz	
	Elevation Plane w/o gnd plane	4C-27

Transmitter Spectrums

Mode CW

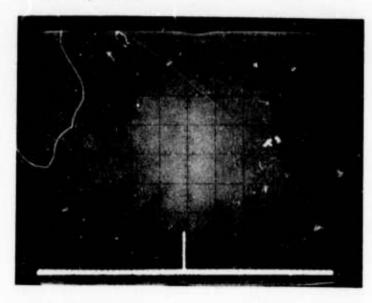


1325 MHz



LOG REF +10 DBM BW 300 KHZ FC 1325 MHZ SCAN 20 MHZ/DIV

Standby Mode



XMTR
-30 DB
SPECTRUM
ANALYZER

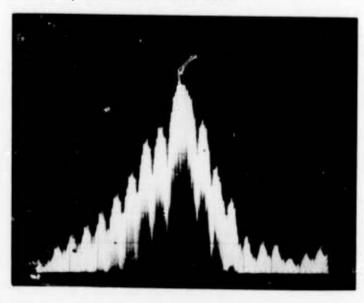
LOG REF +10 DBM
BW 300 KHZ
FC 1325 MHZ
SCAN 20 MHZ/DIV

NOTE

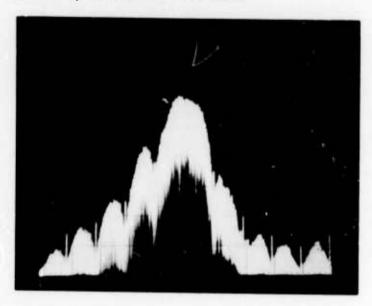
With PA power off, signal is <-50 dBm.

Transmitter Spectrums (Cont)

10 M-Chip Continuous Code Mode



20 M-Chip Continuous Code Mode



$1325~\mathrm{MHz}$



LOG REF +10 DBM BW 300 KHZ

FC 1325 MHZ (APPROX) SCAN 20 MHZ/DIV

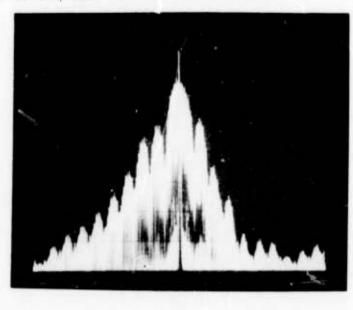
XMTR 30 DB
SPECTRUM
ANALYZER

LOG REF +10 DBM BW 300 KHZ

FC 1325 MHZ (APPROX) SCAN 20 MHZ/DIV

Transmitter Spectrums (Cont)

10 M-Chip Rate 1 Code/1 Carrier Mode

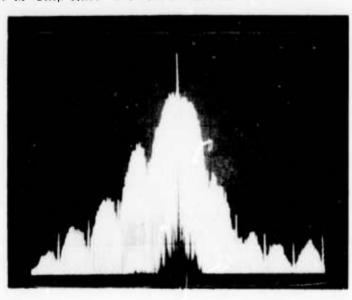


1325 MHz



LOG REF +10 DBM BW 300 KHZ FC 1325 MHZ SCAN 20 MHZ/DIV

20 M-Chip Rate 1 Code/1 Carrier

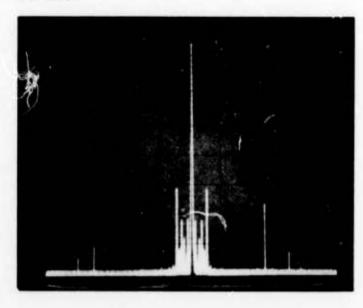


XMTR
30 DB
SPECTRUM
ANALYZER

LOG REF +10 DBM BW 300 KHZ FC 1325 MHZ SCAN 20 MHZ/DIV

Transmitter Spectrums

CW Mode

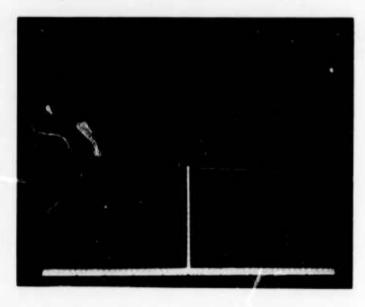


430 MHz



LOG REF +10 DBM BW 300 KHZ FC 430 MHZ SCAN 20 MHZ/DIV

Standby Mode





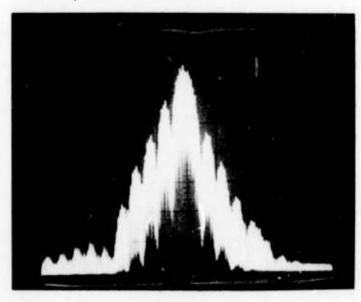
LOG REF +10 DBM BW 300 KHZ FC 430 MHZ SCAN 20 MHZ/DIV

NOTE

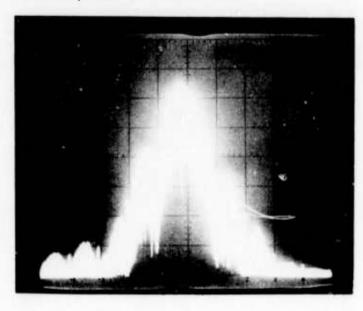
With PA power off, signal is <-80 dBm.

Transmitter Spectrums (Cont)

10 M-Chip Rate Continuous Code



20 M-Chip Rate Continuous Code



$430~\mathrm{MHz}$



EOG REF +10 DBM BW 300 KHZ FC 430 MHZ SCAN 20 MHZ/DIV

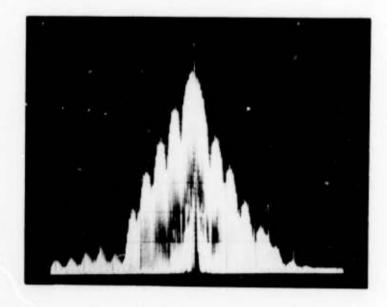
XMTR 40 DB

SPECTRUM ANALYZER

LOG REF +10 DBM BW 300 KHZ FC 430 KHZ SCAN 20 MHZ/DIV

Transmitter Spectrums (Cont)

10 M-Chip Rate 1 Code/1 Carrier

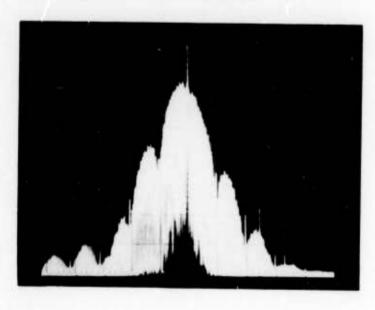


 $430~\mathrm{MHz}$



LOG REF +10 DBM BW 300 KHZ FC 430 MHZ SCAN 20 MHZ/DIV

20 M-Chip Rate 1 Code/1 Carrier



LOG REF +10 DBM BW 300 KHZ FC 430 MHZ SCAN 20 MHZ/DIV

Received Signals

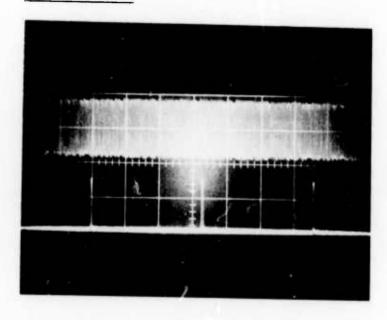
The following apply for this series of pictures:

- Top Trace rf if. measured at threshold detector output (0.5V/cm)
- Bottom Trace envelope detector output (1.0V/cm)

(Measurements taken on Tektronix's 585A.)

- Horizontal Scale 4 µs/cm
- Transmitter rf attn'd & connected to receiver
- AGC in manual gain.

10 M-Chip Rate



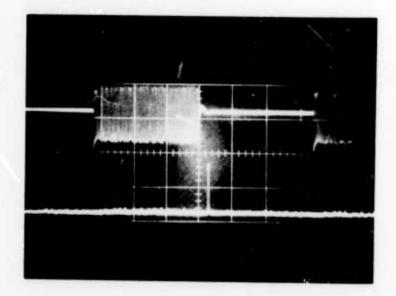
CONTINUOUS PRN CODE

05 V/CM (VERT)

DET 1.0 V/CM (VERT)

Receive Signals

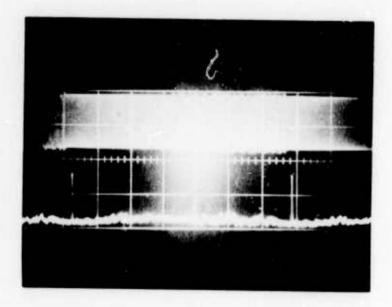
10 M-Chip Rate (Cont)



1 CODE - 1 BLANK

<u>IF</u>

DET



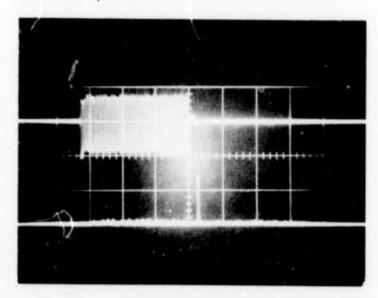
1 CODE - 1 CARRIER

<u>IF</u>

DET

Receive Signals

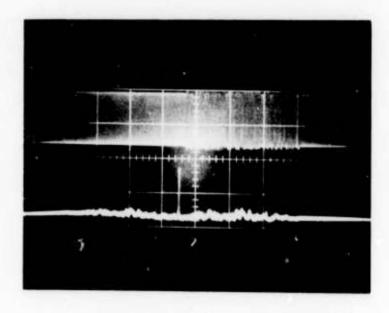
10 M-Chip (Cont)



1 CODE - 3 BLANK

IF

DET



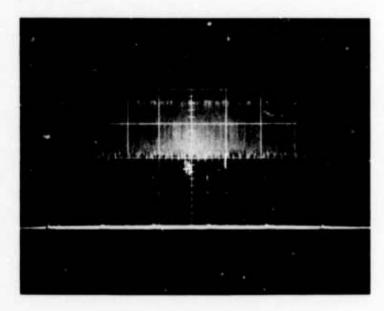
1 CODE - 3 CARRIER

<u>IF</u>

DET

Receive Signals

20 M-Chip



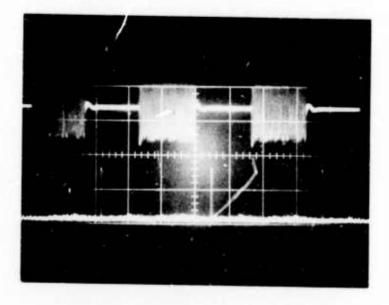
CONTINUOUS CODE

<u>IF</u>

DET

Receive Signals

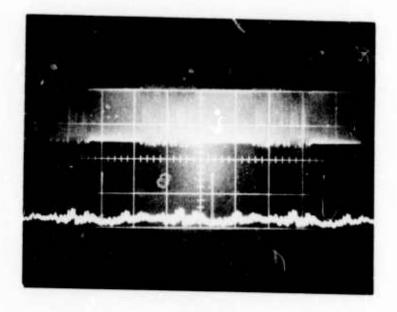
20 M-Chip (Cont)



1 CODE 1 BLANK

IF

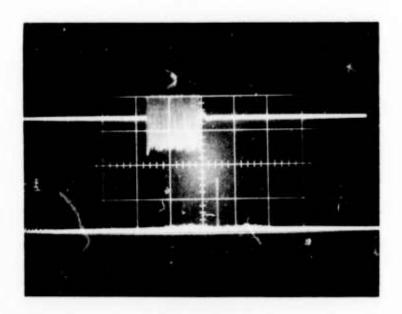
DET



1 CODE 1 CARRIER

IF

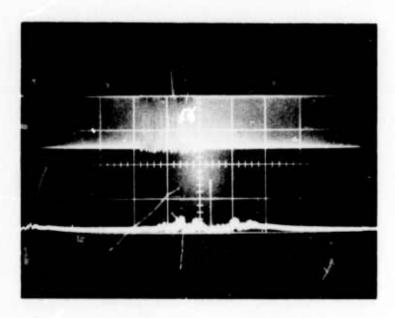
DET





IF

DET

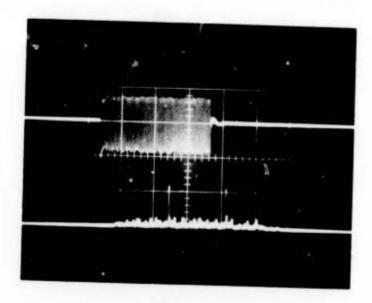


1 CODE = 3 CARRIER

IF

DET

Interaction of SAWD's and Code Rate





10 M CHIP, 1 CODE 3 BLANK

RCVR

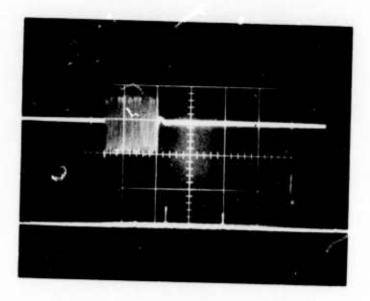
20 M CHIP SAWD RCV

TOP TRACE

RCV IF 0.5 V/CM

BOTTOM TRACE 10 V/CM

TIME BASE 4 µS CM



XMTR

20 M CHIP, 1 CODE 3 BLANK

RCVR

10 M CHIP SAWD RCV

TOP TRACE

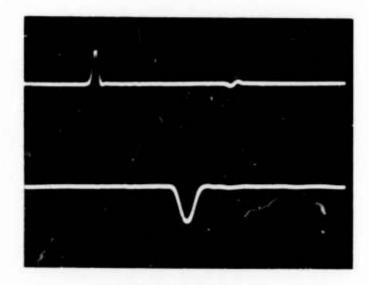
RCV IF 05 V CM

BOTTOM TRACE 1.0 V CM

TIME BASE 4 parCM

Miscellaneous Radio Data

Envelope Detector Response

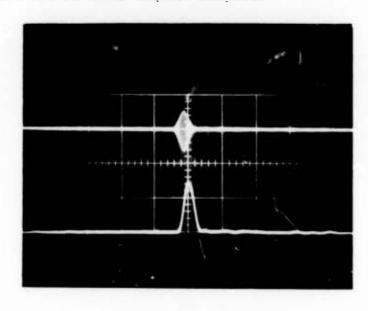


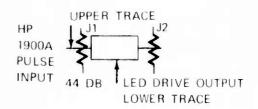


10 M-CHIP 1 CODE 3 BLANK
TOP TRACE SAWD OUTPUT
0.5 V/CM (AT THRESHOLD
DET OUTPUT)
BOTTOM TRACE ENVELOP DET
OUTPUT 1.0 V/CM

TIME BASE 4 µS/CM

Threshold Detector Impulse Response





TIME BASE 20 NS DIV TOP TRACE 2V/DIV BOTTOM TRACE 2V DIV

TYP OF AN UNSATURATED DETECTOR

THE DELAY BETWEEN
INPUT & OUTPUT NOT VALID DUE
TO TEST SETUP

